

Reduced Order Physics Capacitance Resistance Models

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Hypothesis



Characteristics of a reservoir can be inferred from analyzing production and injection data only.



CRM for an Injector-Producer Pair

Continuity:

$$c_t V_p \frac{d\bar{p}}{dt} = I(t) - q(t)$$

Production Rate:

$$q(t) = J(\bar{p} - p_{wf})$$

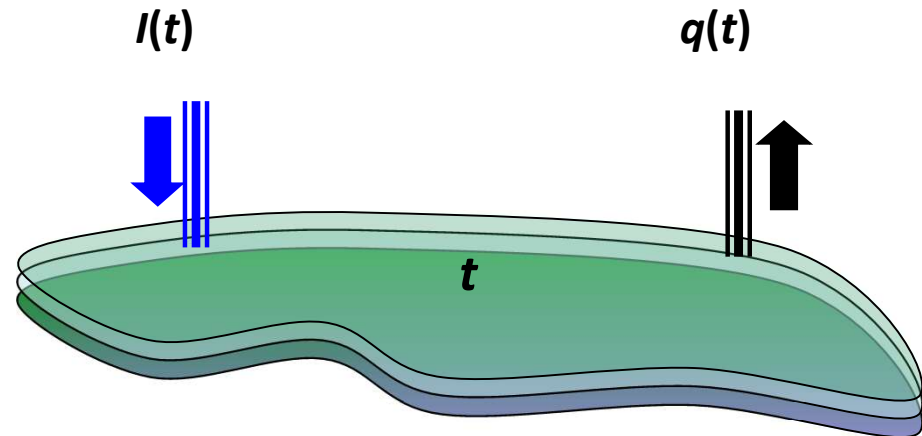
"Pressure is a reservoir engineer's best friend"
Fokert Brons

Combine to form

Ordinary Differential Equation:

$$\frac{dq(t)}{dt} + \frac{1}{\tau} q(t) = \frac{1}{\tau} I(t) - J \frac{dp_{wf}}{dt}$$

Time constant: $\tau = \frac{c_t V_p}{J}$



Primary Production Injection

BH pressure change

Analytic Solution

$$q(t_k) = q(t_{k-1}) e^{-\frac{\Delta t}{\tau}} + \left(1 - e^{-\frac{\Delta t}{\tau}}\right) I(t_k) - J(p_{wf}(t_k) - p_{wf}(t_{k-1})) e^{-\frac{\Delta t}{\tau}}$$

novel idea for a persistent challenge in reservoir engineering... lack of geologic data

Bruce (1943)

SPE 414, Wahl et al. (1962)

An Electrical Device for Analyzing Oil-reservoir Behavior

By W. A. BRUCE, * JUNIOR MEMBER A.I.M.E.

(Austin Meeting, October 1942)

ABSTRACT

This paper covers the theory and present state of development of an apparatus for the nonmathematical analysis of complex problems

the block can be used. In analyzing reservoir behavior from this point of view by mathematical means, a set of simultaneous difference equations would be obtained

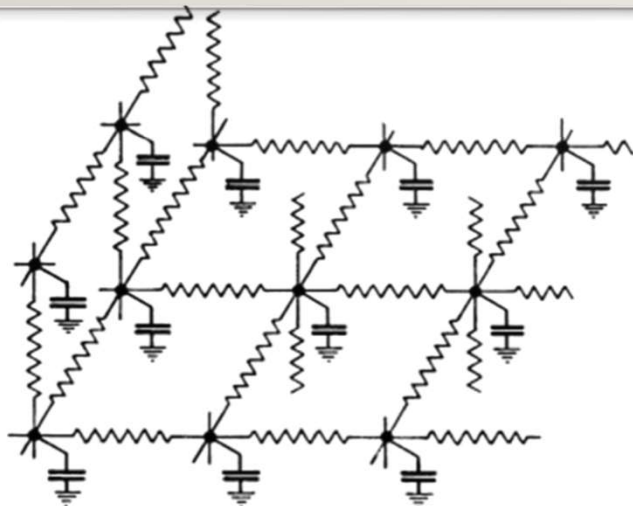


FIG. 3.—PART OF THREE-DIMENSIONAL ELECTRICAL REPRESENTATION

Matching the Performance of Saudi Arabian Oil Fields

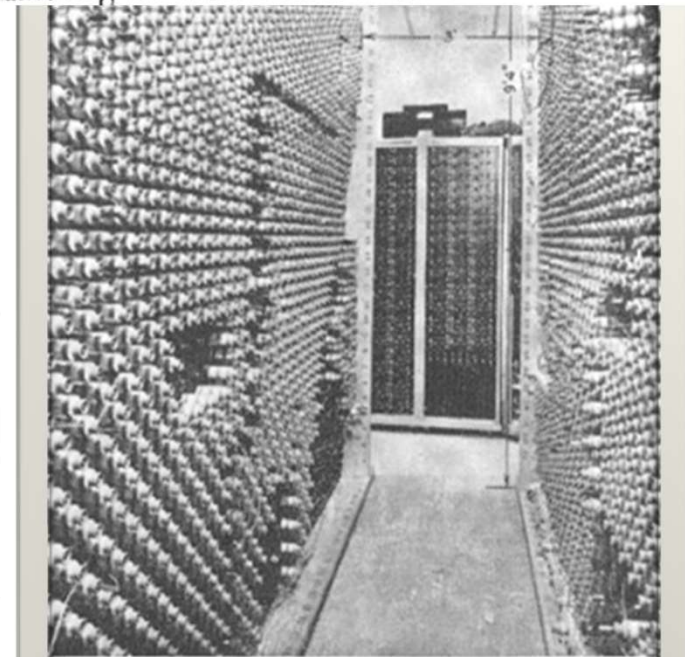


FIG. 1—INSIDE VIEW OF "TUNNEL" FORMED BY THE TWO SECTIONS OF THE MODEL'S RESISTOR-CAPACITOR (RC) NETWORK

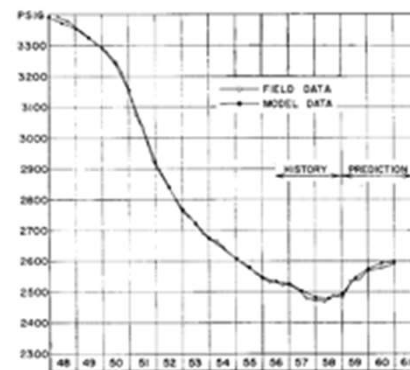


FIG. 14—COMPARISON OF MODEL PRESSURE AND FIELD PRESSURE FOR CONTROLLER 4, NORTHERN ABQAIQ FIELD

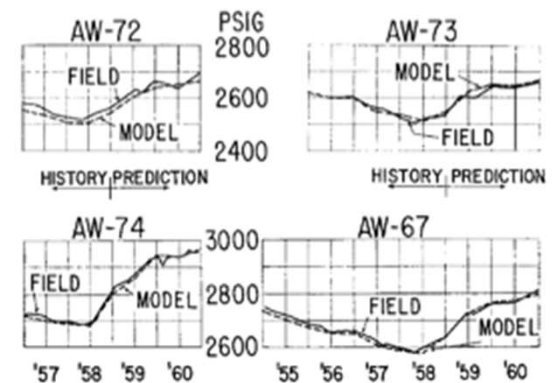
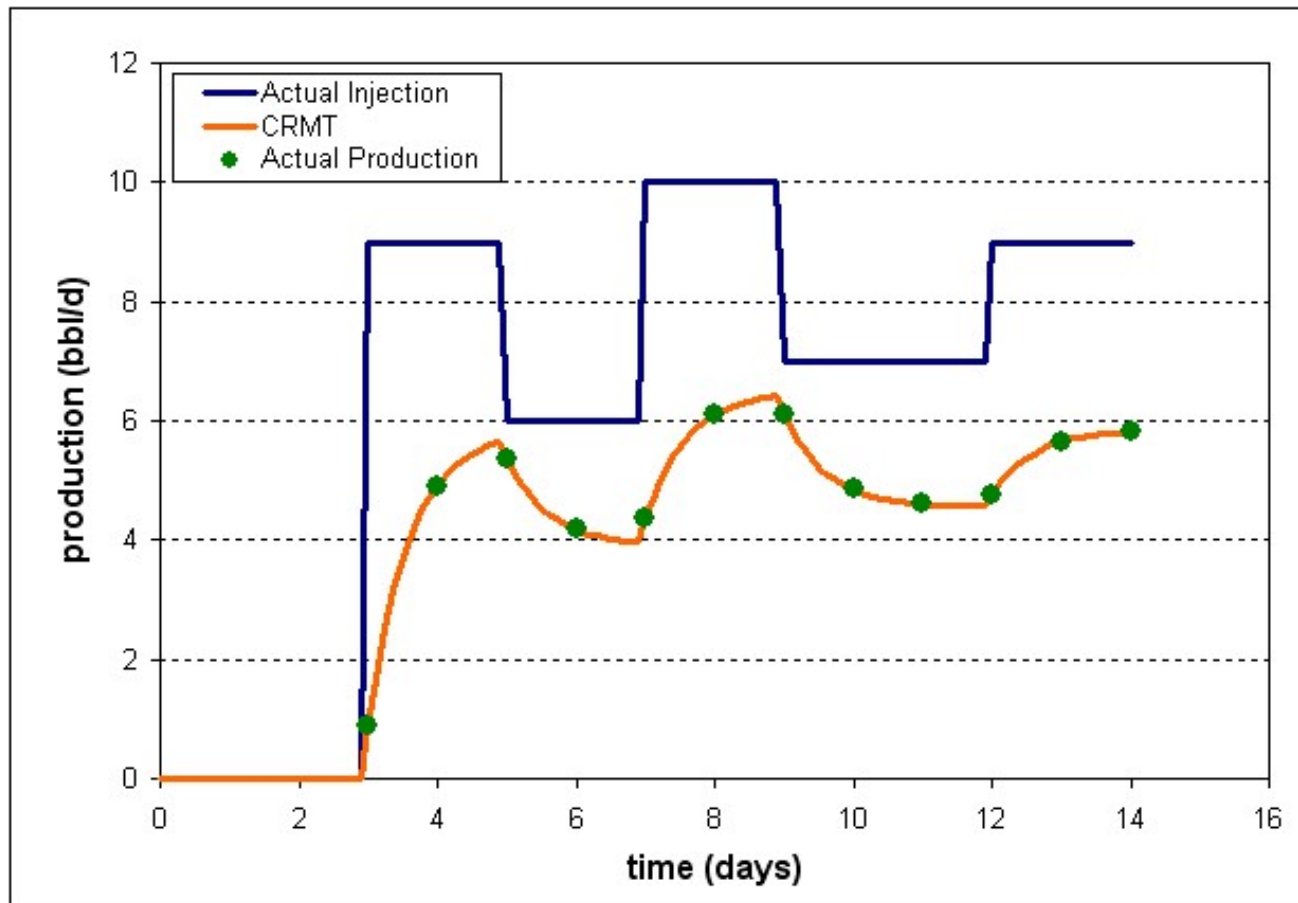


FIG. 16—COMPARISON OF MODEL VS. FIELD BOTTOM-HOLE PRESSURES FOR FOUR ABQAIQ WELLS

Signal Response

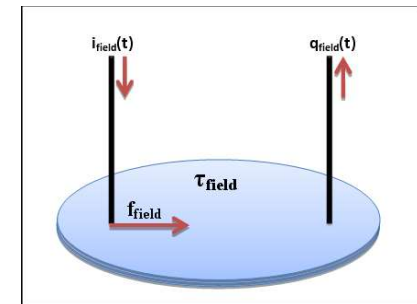
Production response to an injection signal



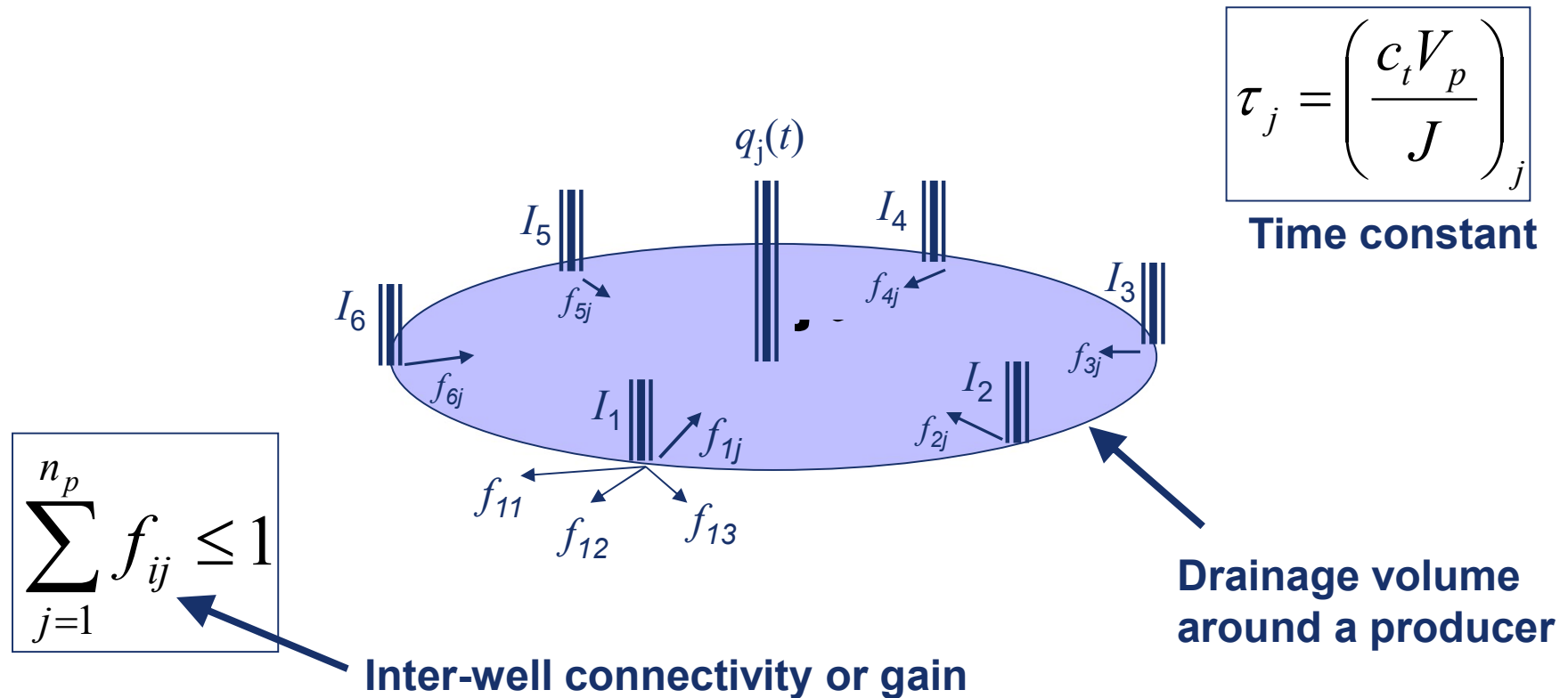
Connectivity

$$\tau_{ij} = 6 \text{ days}$$

$$f_{ij} = 65\%$$



Capacitance-Resistance Model (CRMP)



$$q_{jk} = q_{j(k-1)} e^{-\Delta t / \tau_j} + \left(1 - e^{-\Delta t / \tau_j} \right) \sum_{i=1}^{n_i} f_{ij} I_{ik}$$

Comparisons.....

Conventional world

$$\frac{1}{\alpha} \frac{\partial P}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial P}{\partial r} \right)$$

$$\alpha = \frac{k}{\mu \phi c_t}$$

k, ϕ world

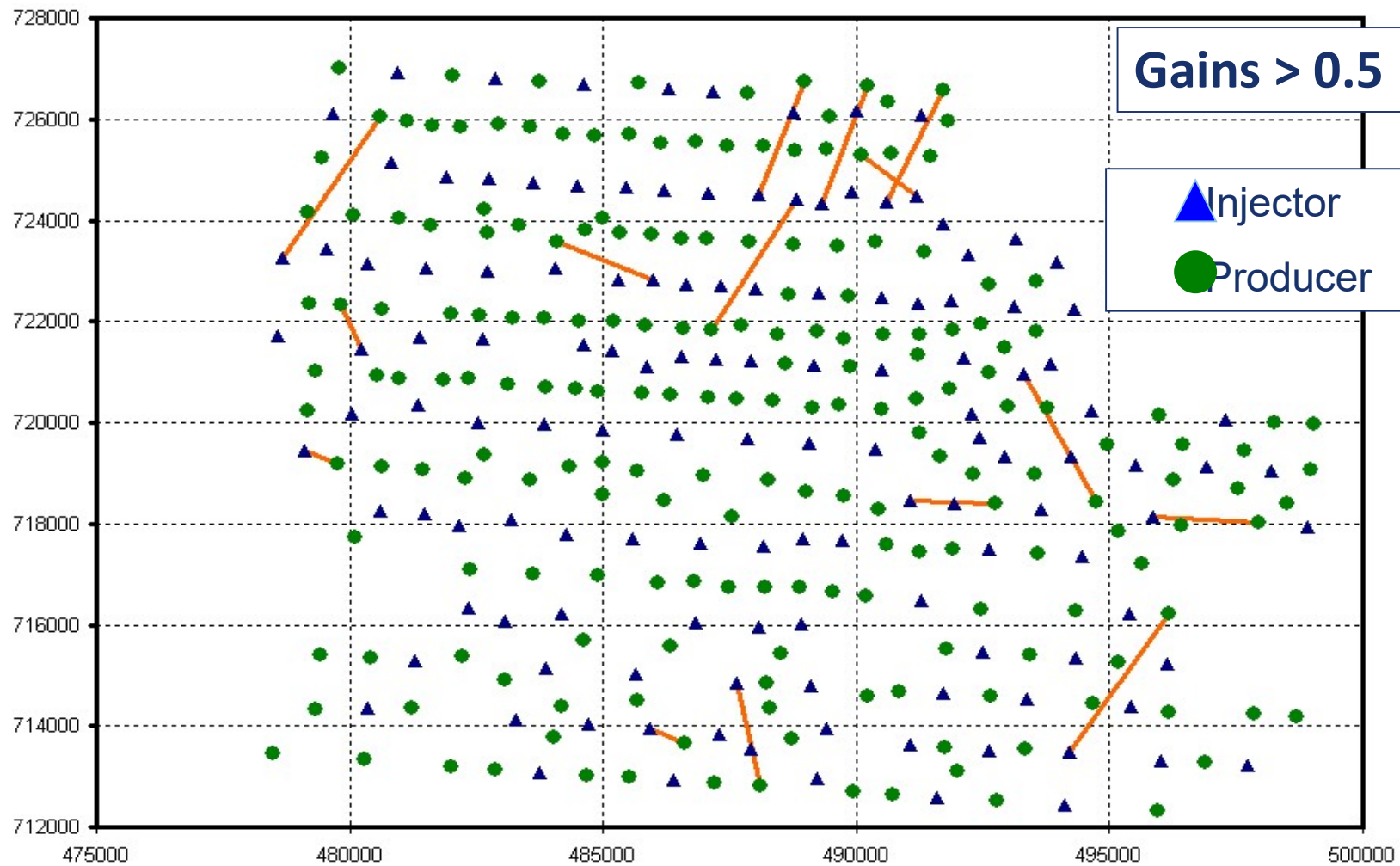
CRM world

$$c_t V_p \frac{d\bar{P}}{dt} = i(t) - q(t)$$

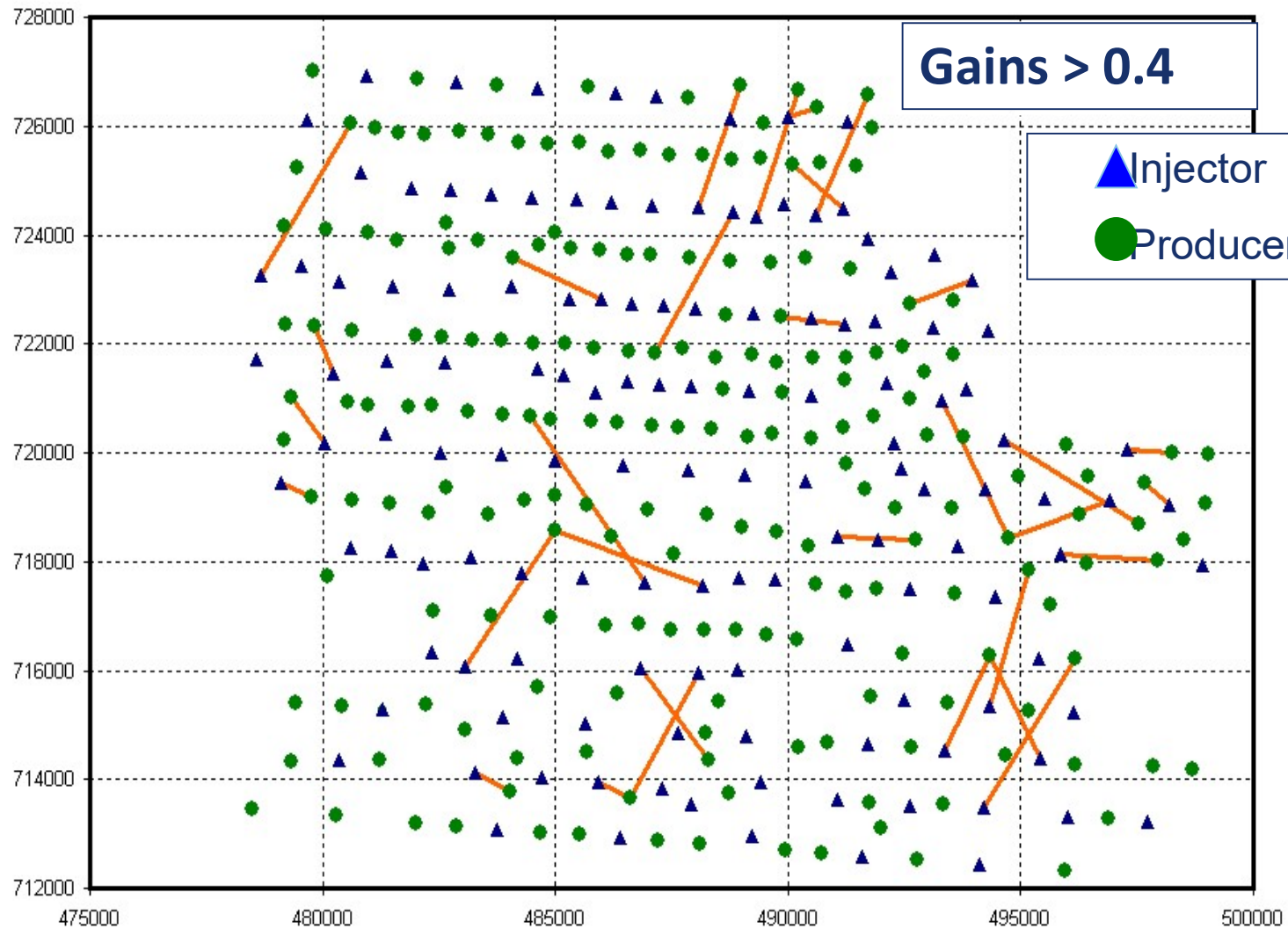
$$q = J(\bar{P} - P_{wf})$$

τ, V_p world

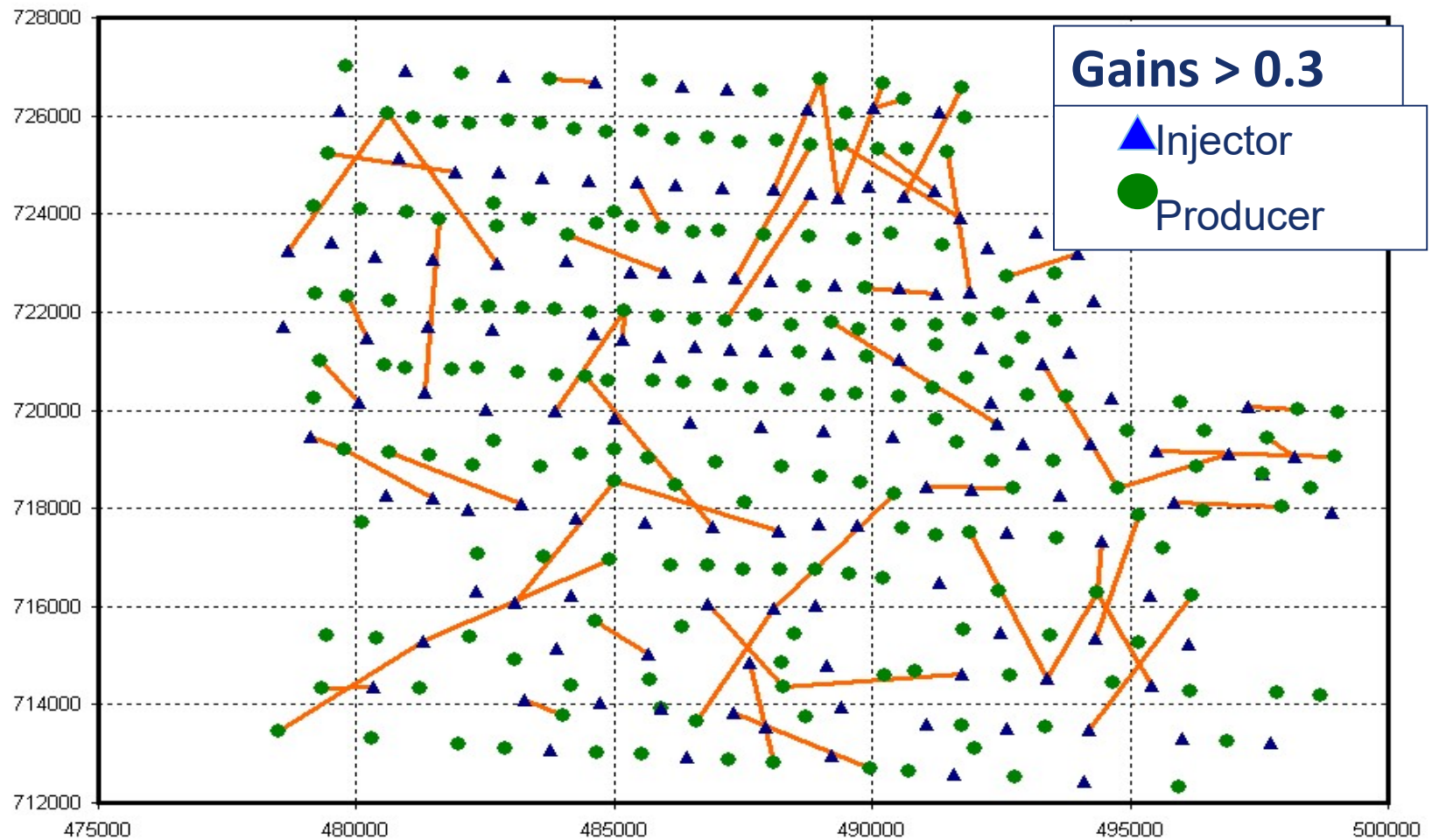
Mature West Texas Waterflood



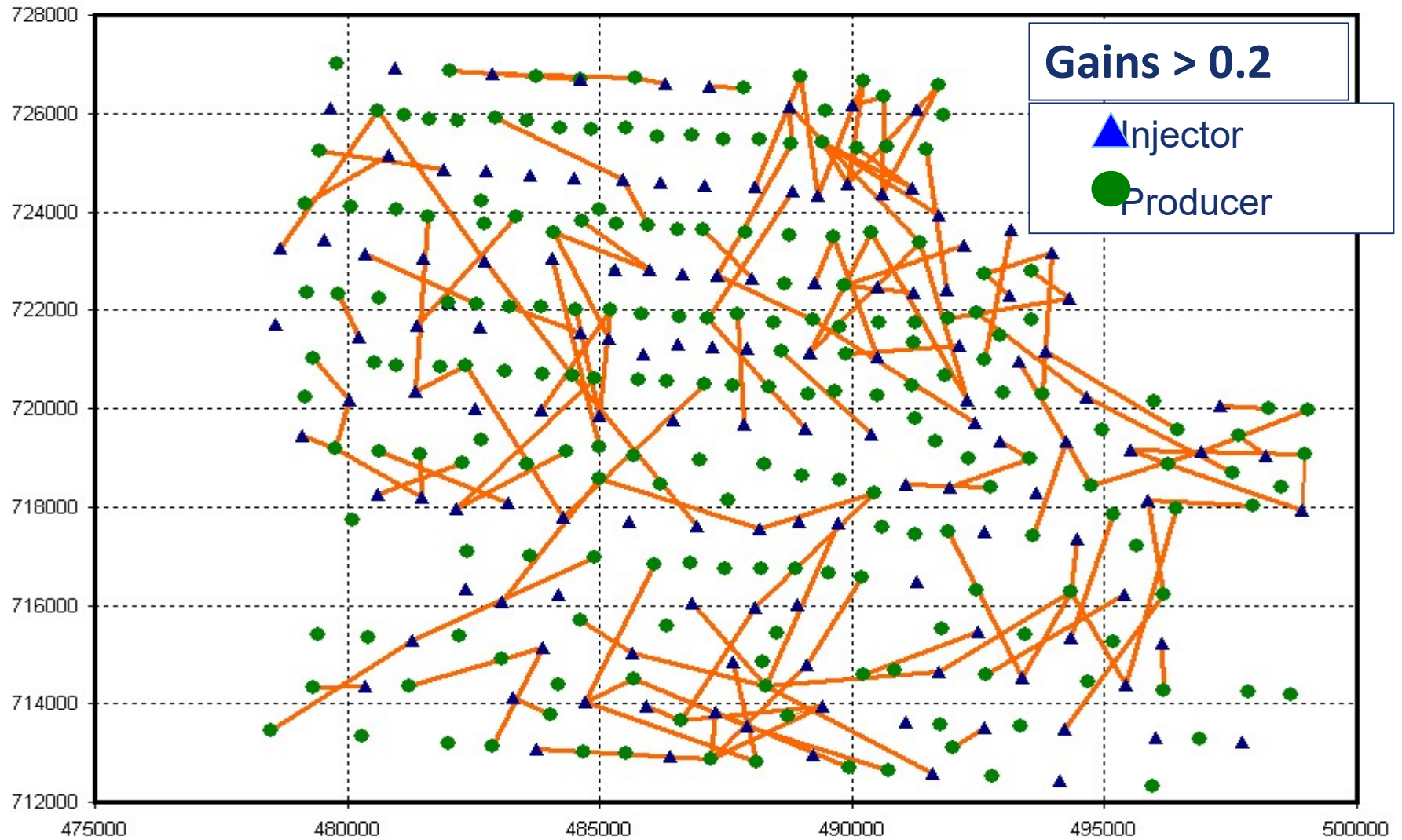
Mature West Texas Waterflood



Mature West Texas Waterflood

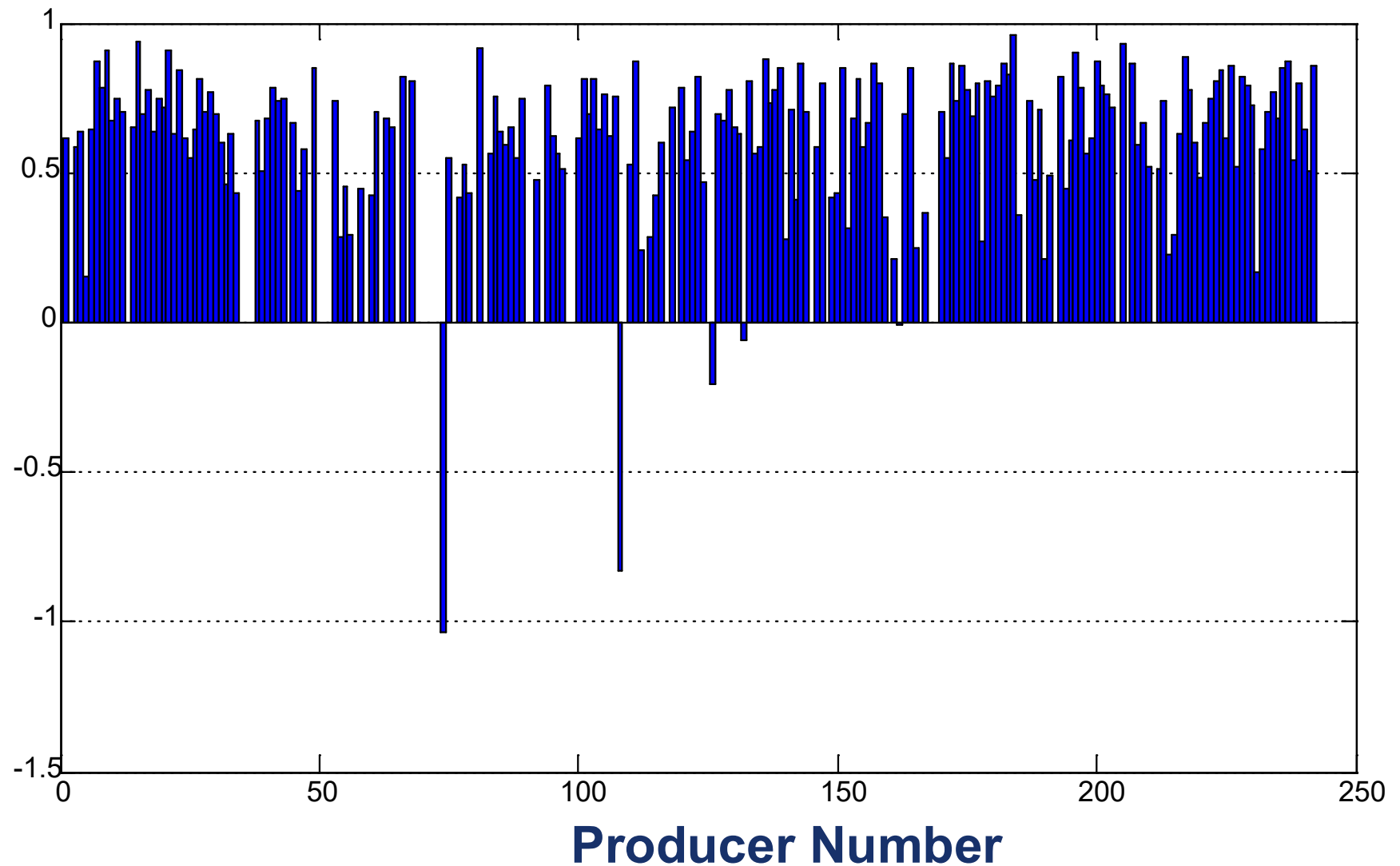


Mature West Texas Waterflood

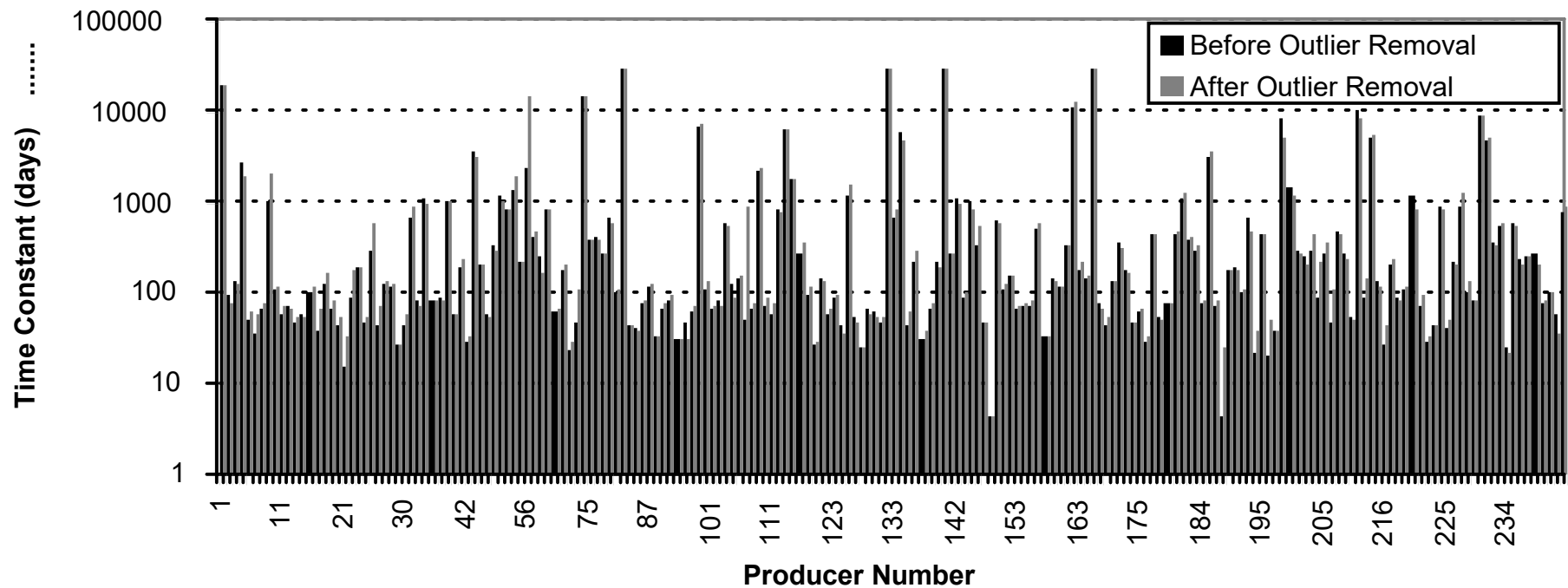


Mature West Texas Waterflood

R-squared

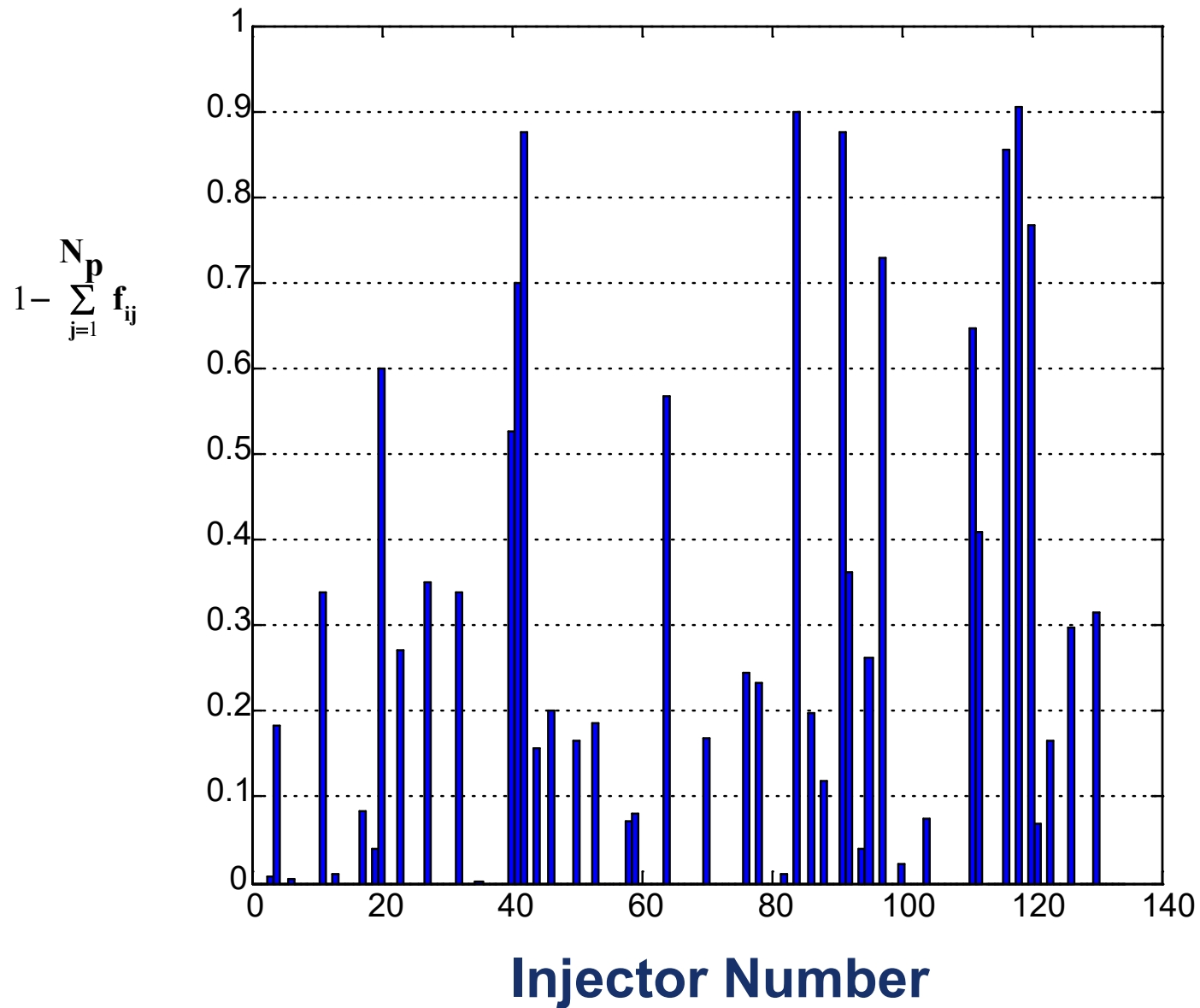


Time Constants



Reservoir A

Lost Injection



Basic Equations



Applications

- Effect of BHP
- Primary production
- CRM and tracers
- Oil rate modeling
- Optimization
- Tracking CO₂ floods
- CRM machine learning



Basic Equations



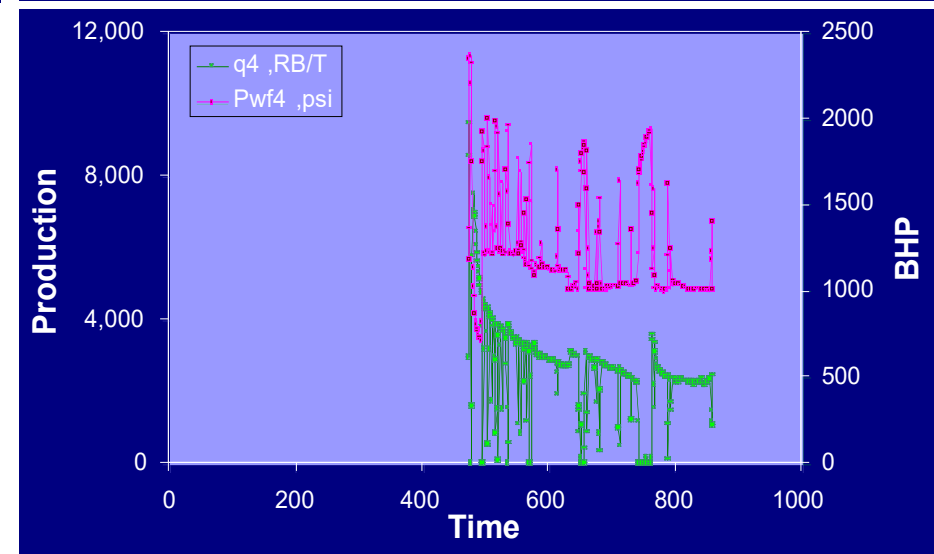
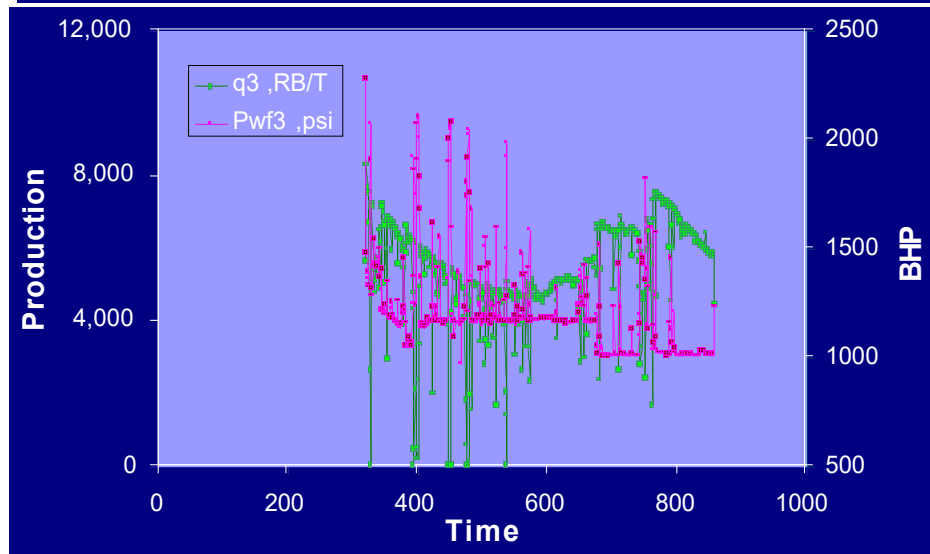
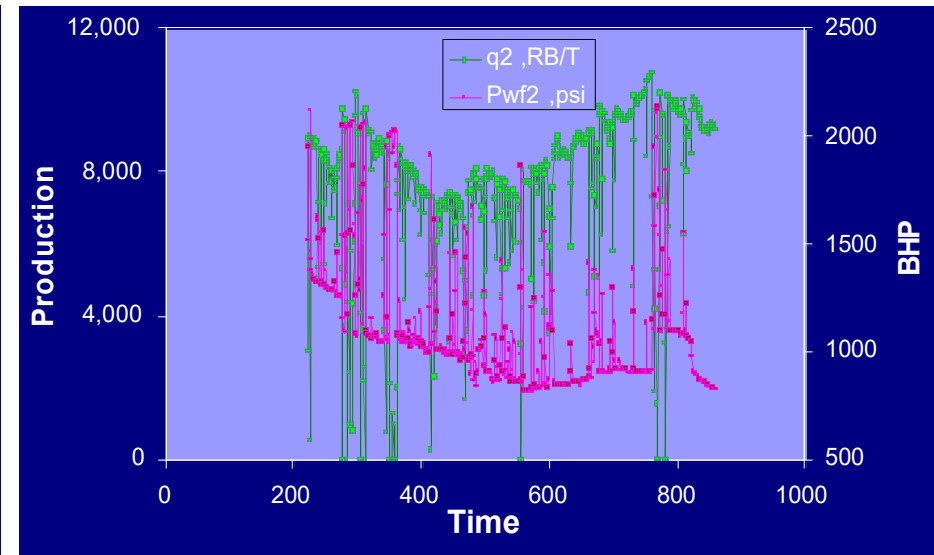
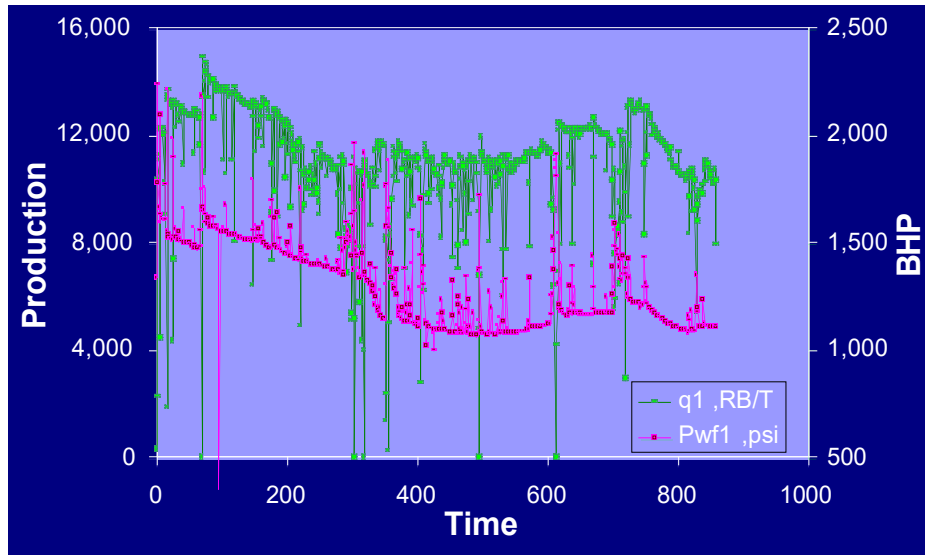
Applications

– Effect of BHP

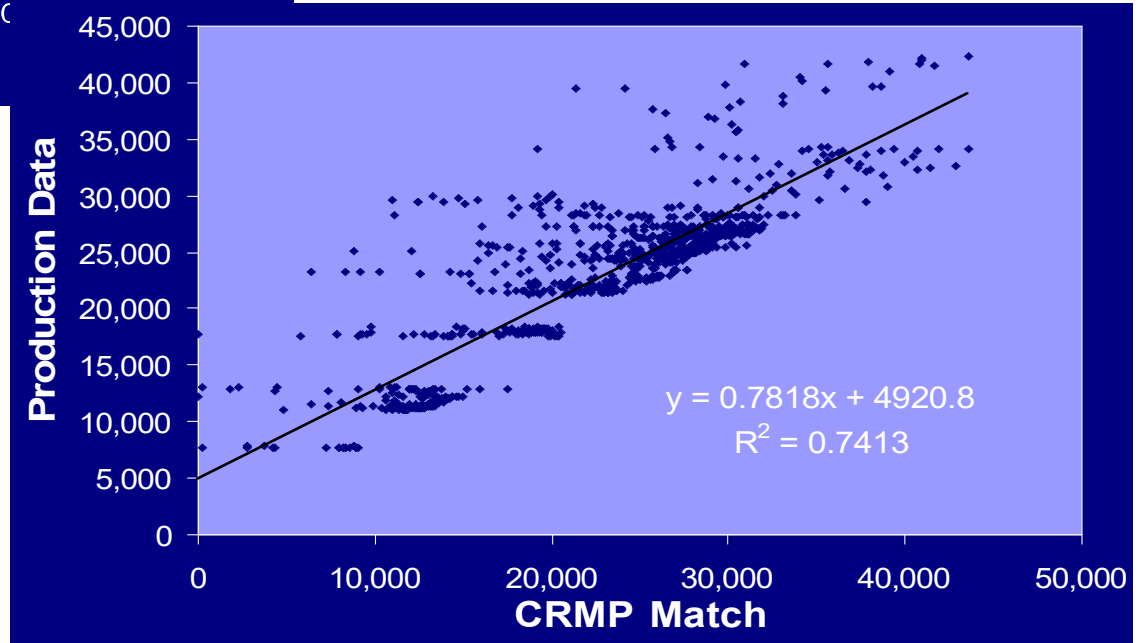
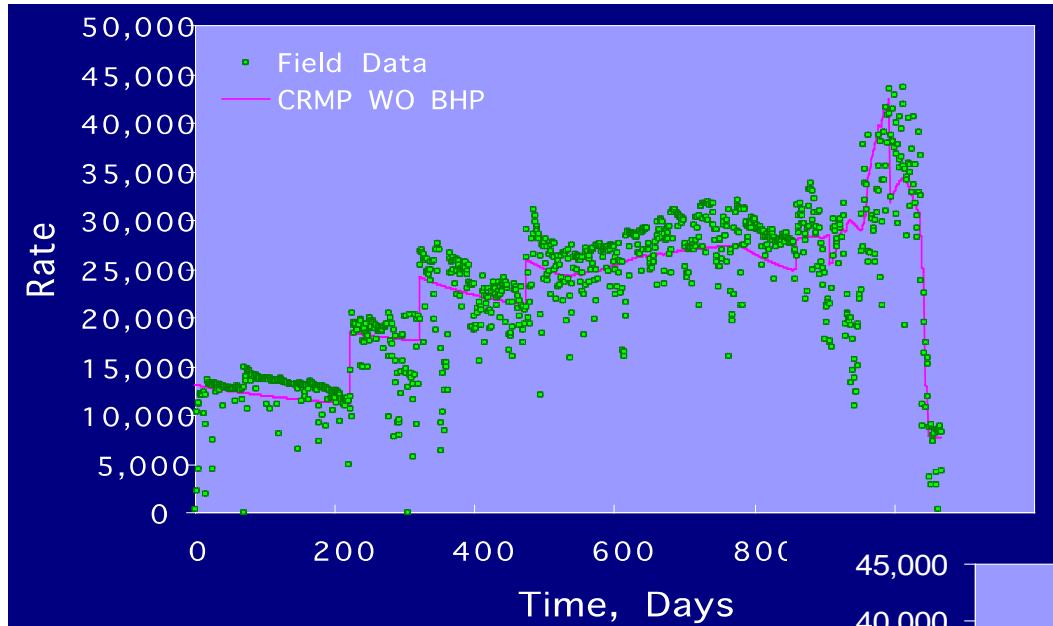


North Sea Case

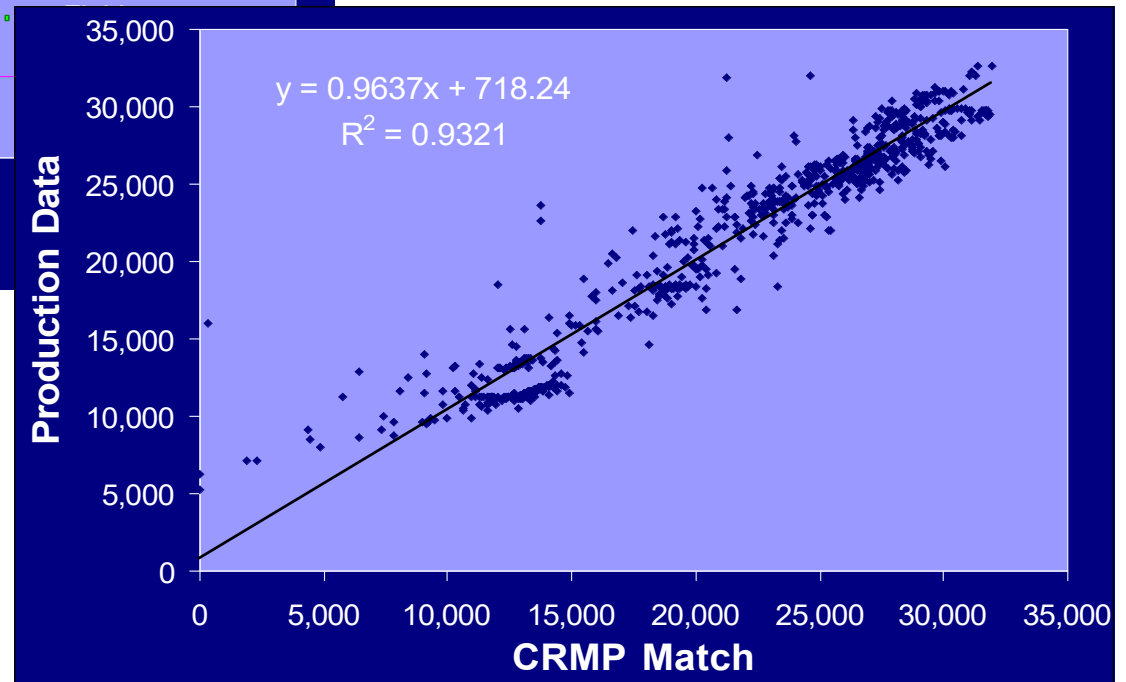
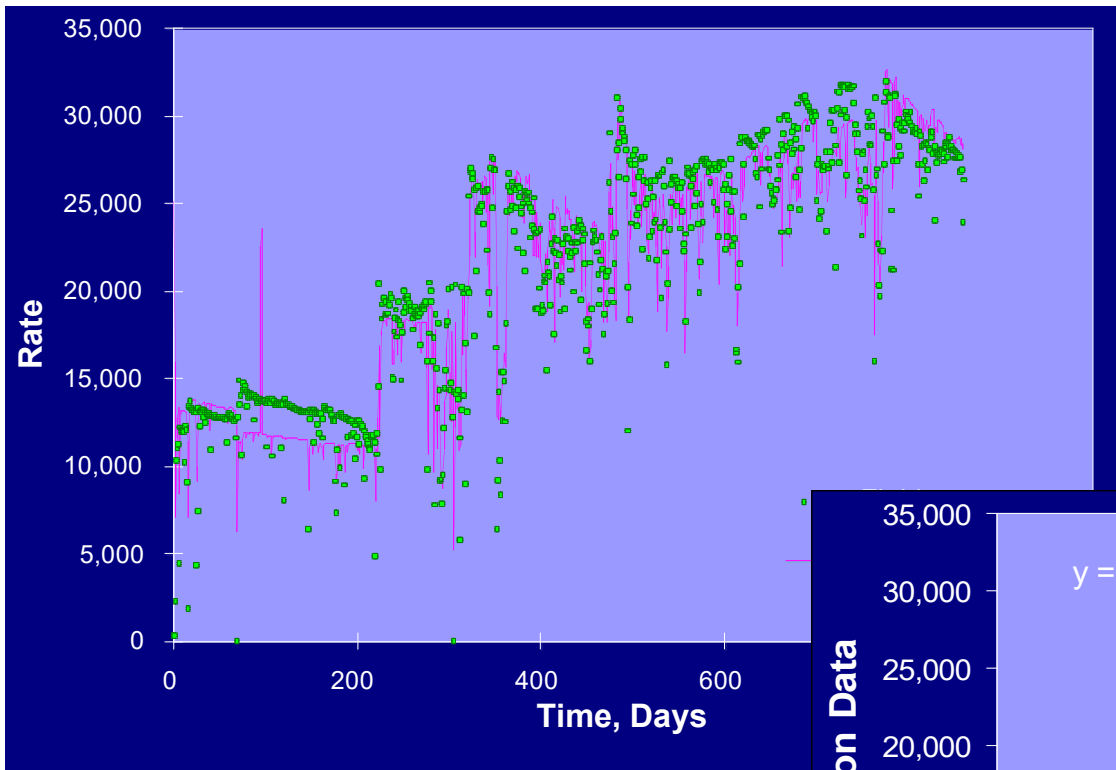
Production and BHP Data



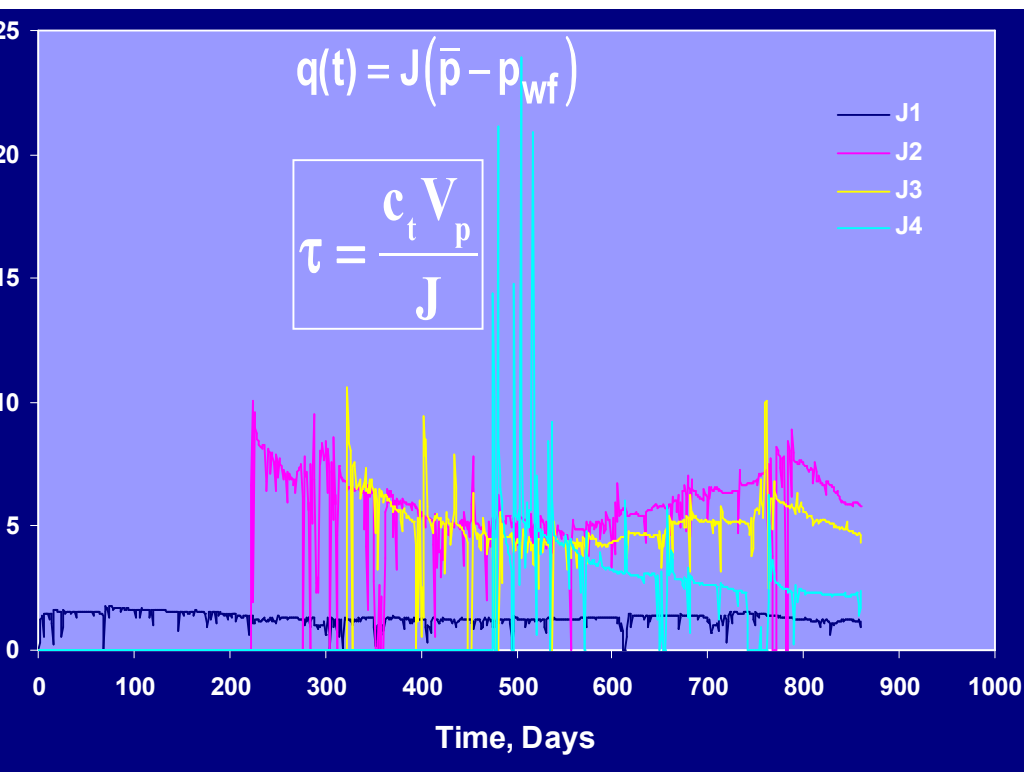
North Sea CRMP wo BHP



North Sea CRMP with BHP



Well Management--Identify Problem Wells



“Pressure is a reservoir engineer’s best friend”
Fokert Brons

- Use productivity indices to evaluate well performance
- Requires pressure data

Basic Equations

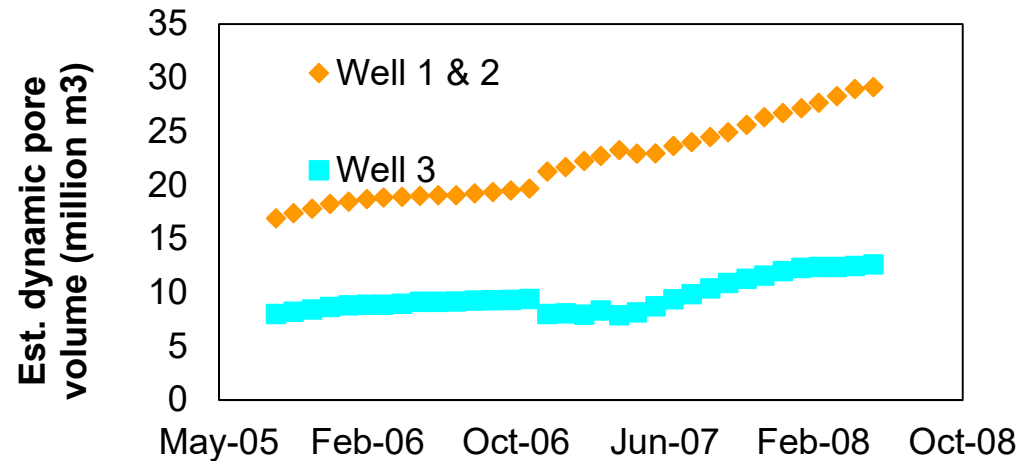


Applications

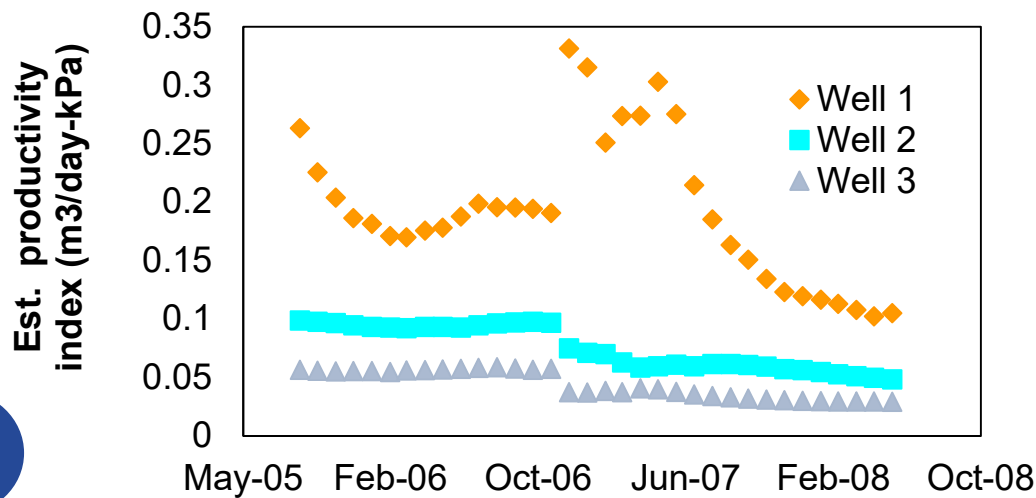
- Effect of BHP
- Primary production



Drainage Volume--Omani Field (primary recovery)



Original oil in place (OOIP) estimated from other methods ranged from 31 to 59 million m³



	Well 1	Well 2	Well 3
$V_p c_t$ (m ³ /kPa)	76.75	74.66	3.25
V_p (10 ⁶ m ³)	15.7	13.4	12.6
J (m ³ /day kPa)	0.09	0.05	0.03
R^2	0.97	0.85	0.91

Basic Equations



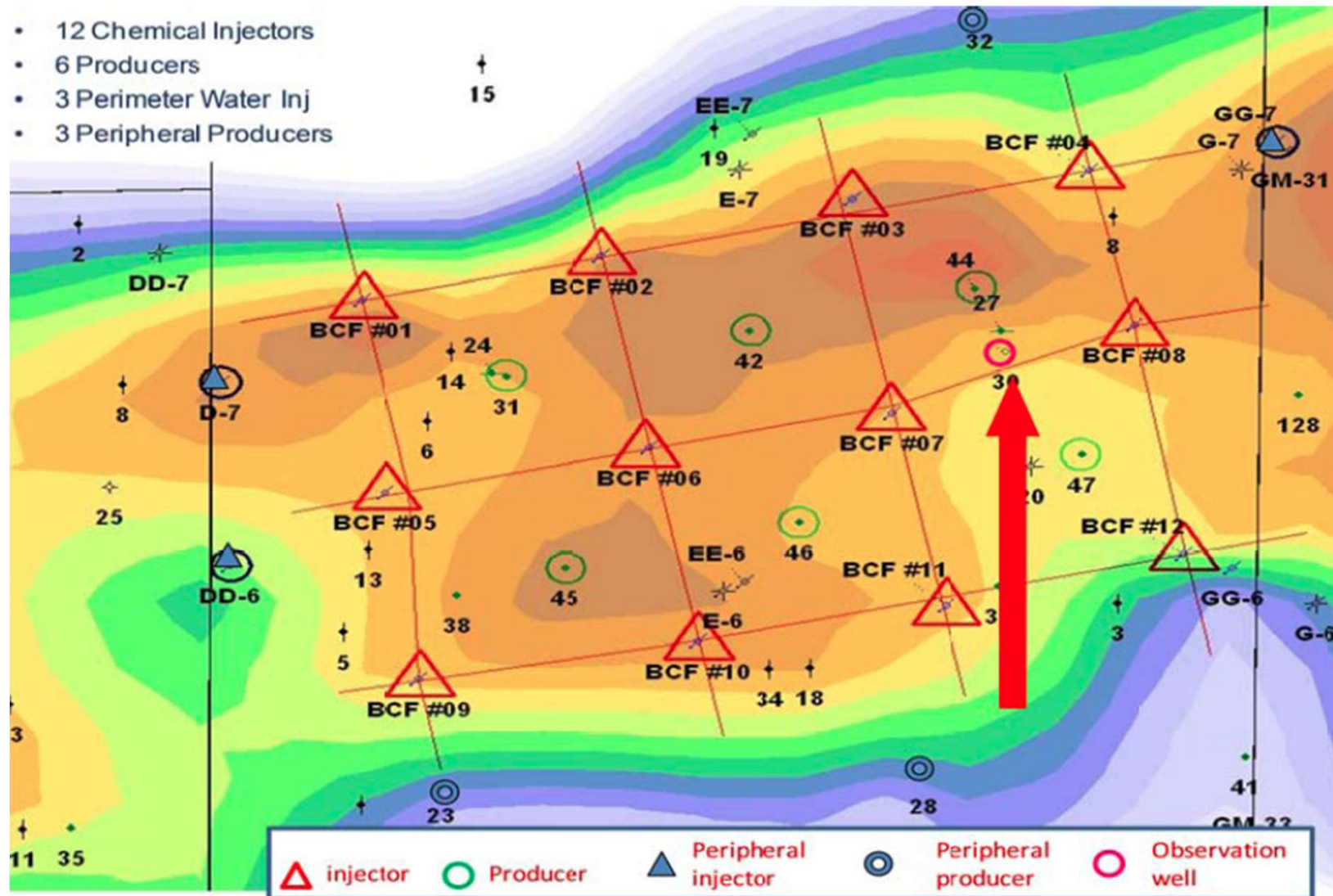
Applications

- Effect of BHP
- Primary production
- CRM and tracers



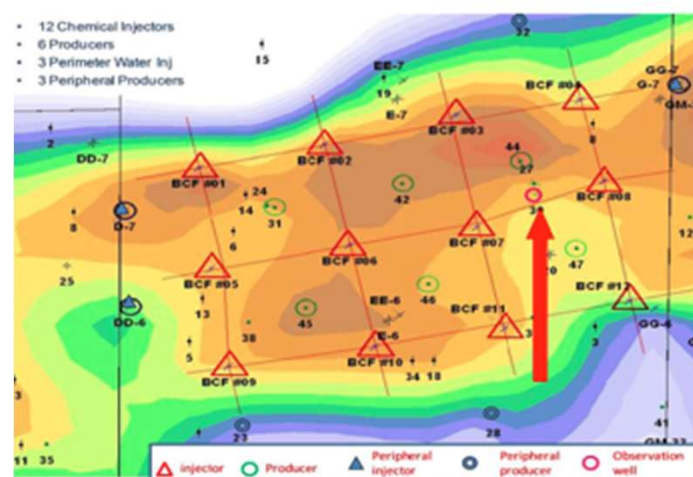
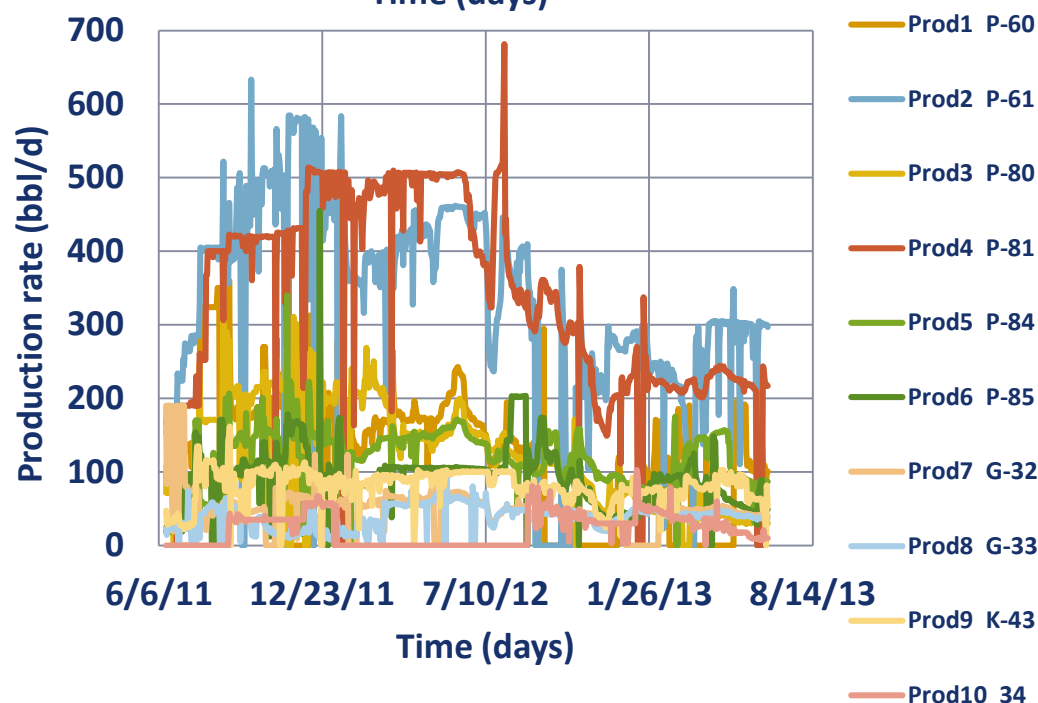
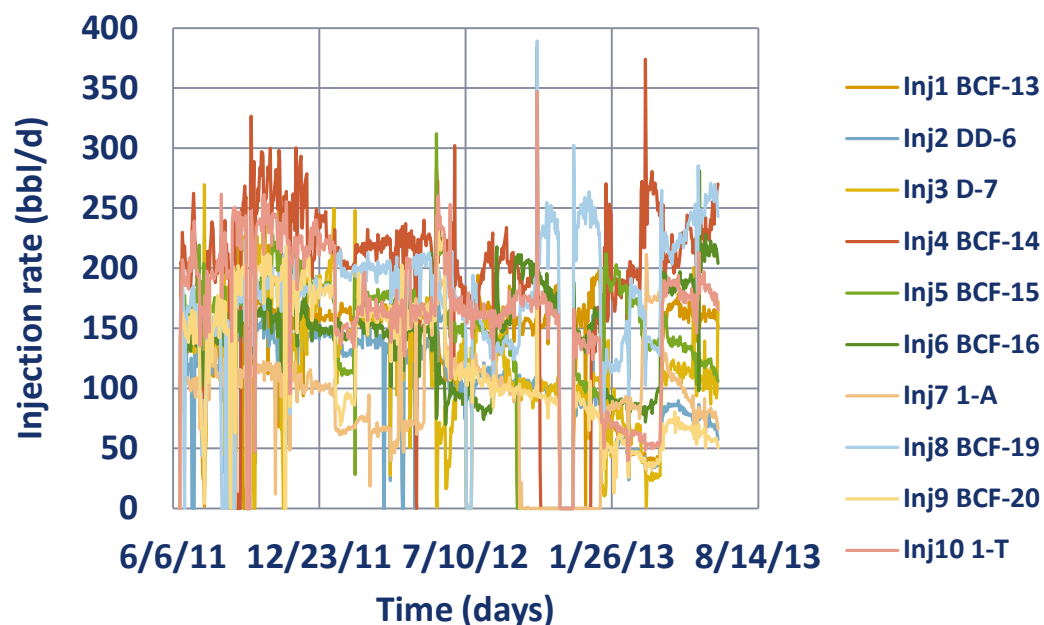
Reservoir Characterization

An alternative to tracers...



Variable Rates

Injection

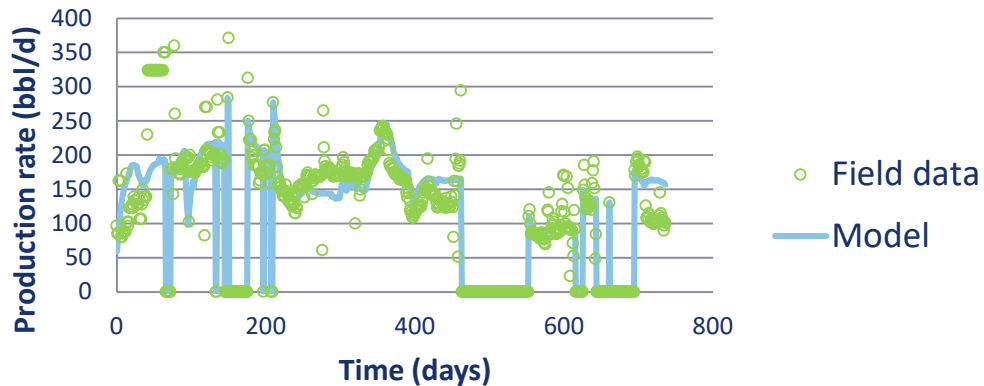


Production

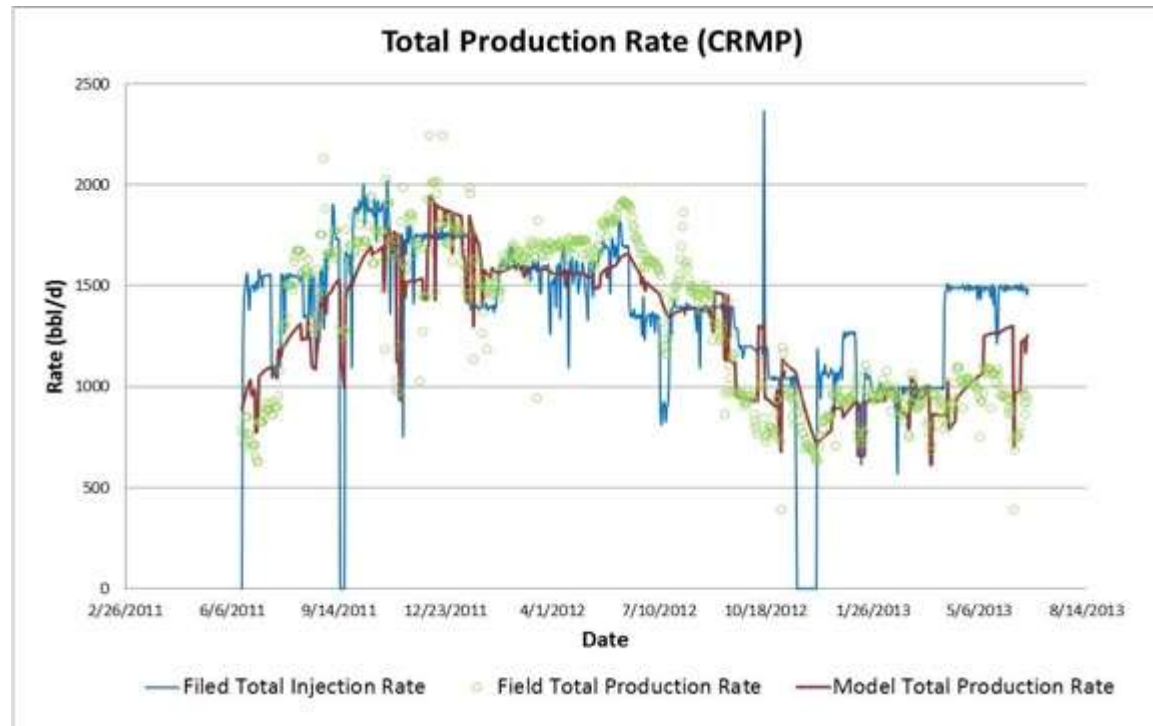
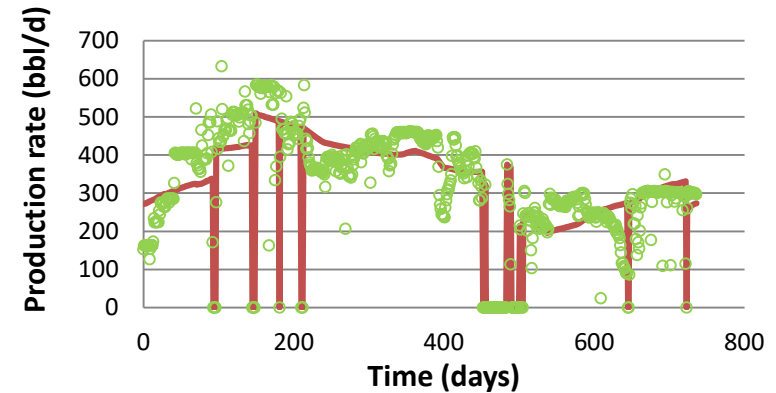
CRM Production History Match

Individual Well and Full Field Matches

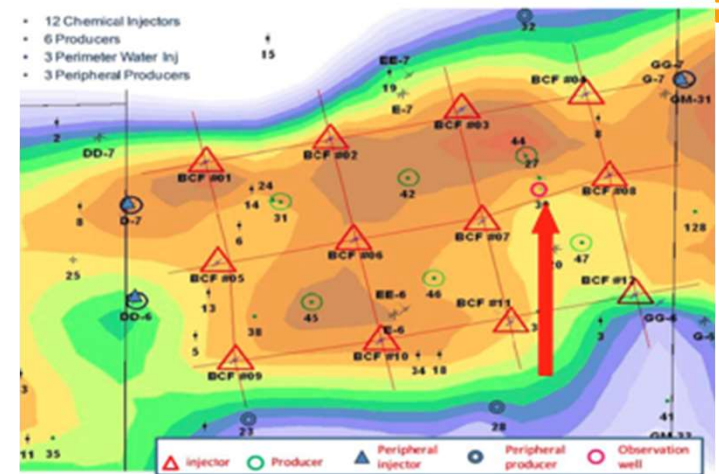
Prod1 (P-60)



Prod2 (P-61)



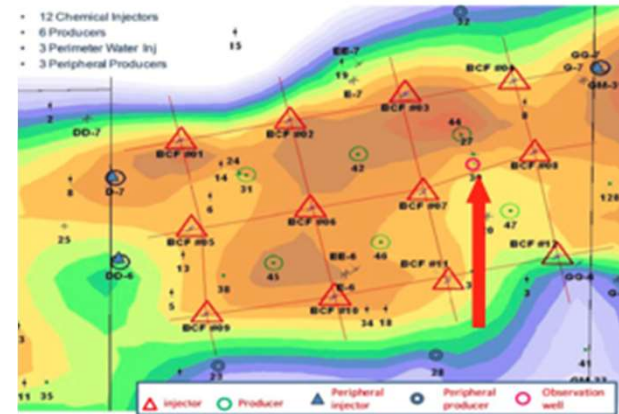
Tracer Performance— How does CRM compare?



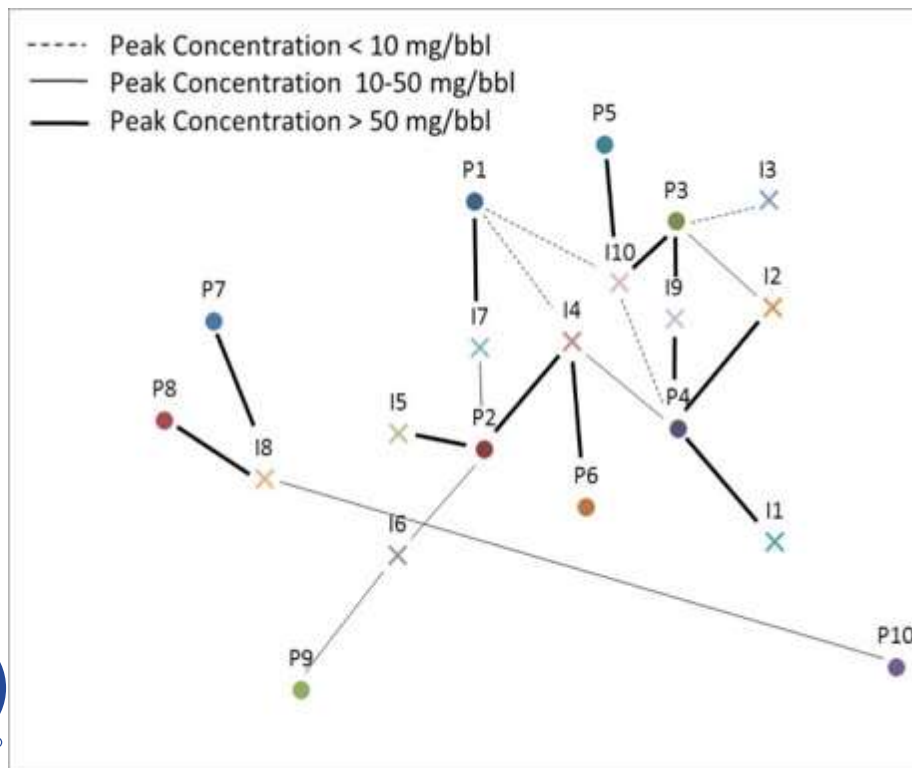
Injector	Tracer	Total injection (gr)	Field data			CRMP + Integrated Model (Simultaneous fitting)	
			Observed in Producer	Total measured produced tracer (gr)	Tracer recovery	Total produced tracer (gr)	Tracer recovery
Inj1	3,4,5-TFBA	6000	P4	3533	59%	3459	58%
Inj2	4-TFMBA	11000	P3, P4	6171	56%	7209	66%
Inj3	3,5-bisTFMBA	7500	P3	115	2%	0	0%
Inj4	2,3,4,5-TFBA	17000	P1,P2,P4,P6	9551	56%	7881	46%
Inj5	2,4,5-TFBA	7500	P2	6472	86%	6517	87%
Inj6	2,4-DFBA 4-FBA	7500	P2,P9	3257	43%	3292	44%
Inj7	2-TFMBA	7500	P1,P2	3034	40%	3815	51%
Inj8	3-TFMBA 2-FBA	7500	P7,P8,P10	2547	34%	2279	30%
Inj9	2,3,4-TFBA	10000	P3, P4	11479	115%	11714	117%
Inj10	2,5-DFBA	7500	P1,P3,P4,P5	4547	61%	5027	67%

Tracer and CRM Results

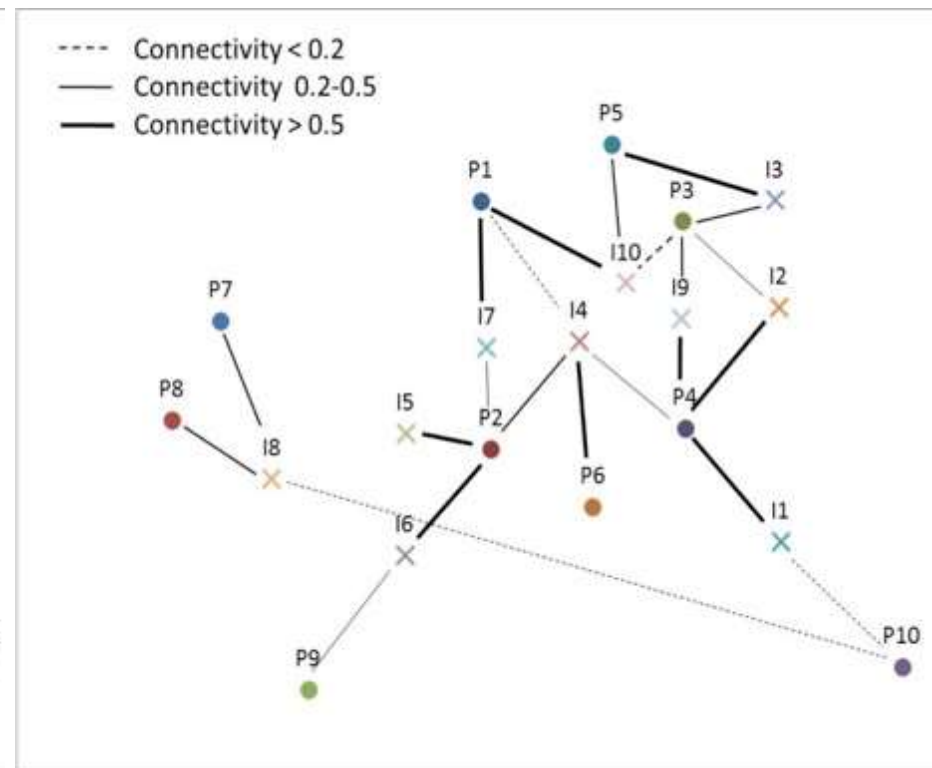
A side by side comparison...



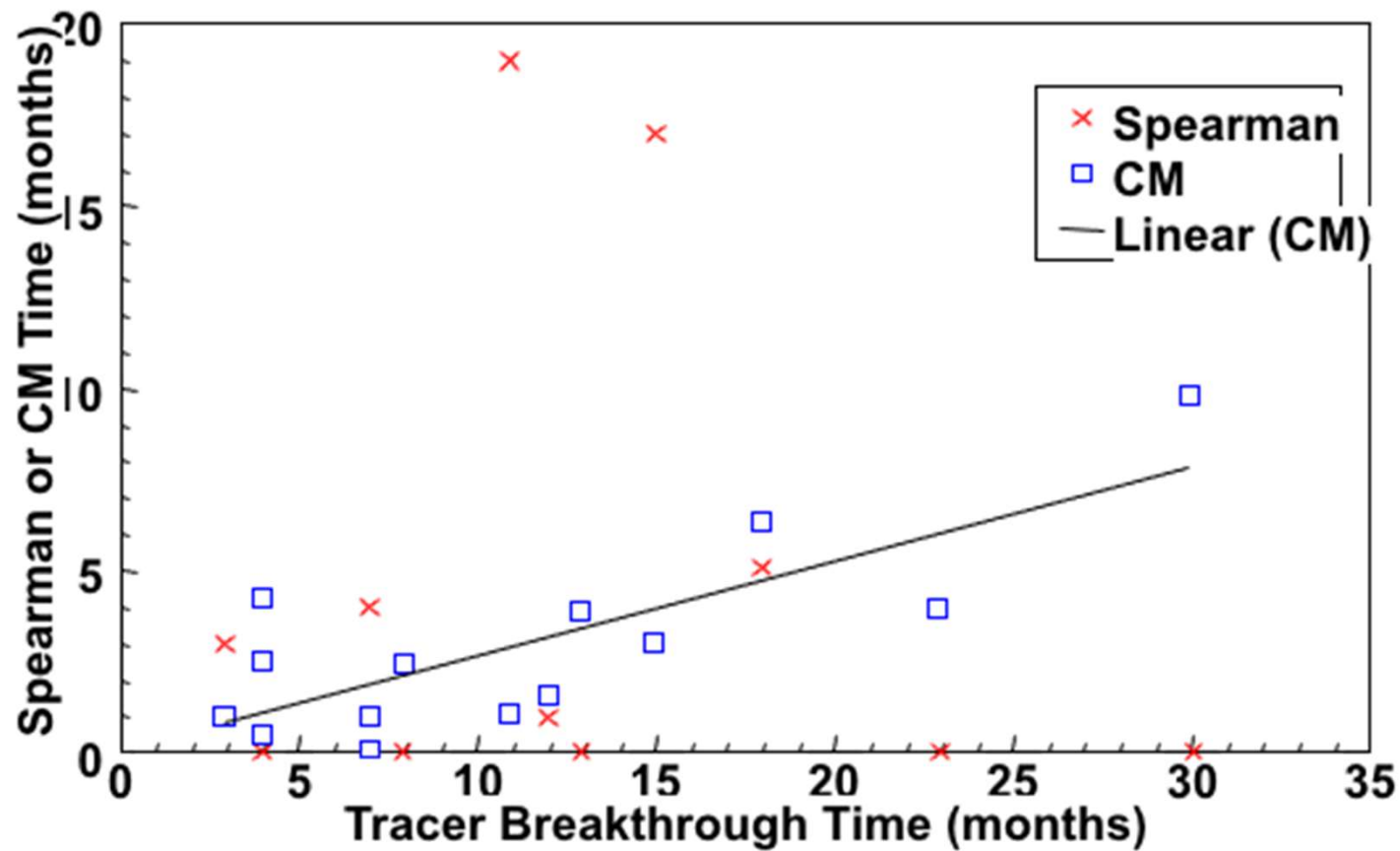
Tracer Peak Concentrations



CRM Allocations



Comparison to Buck Draw Data



Basic Equations



Applications

- Effect of BHP
- Primary production
- CRM and tracers
- Oil rate modeling



Oil Rate Equation

$$q_{oil}(t) = q(t) f_{oil}(t)$$

For each well in CRMP

$$q_{oil}(t) = q(t) (1 - f_{water}(t))$$

	Developed by	Oil Fractional-flow Model	Equation Number
1	Timmermann (1971)	$f_o = \left(1 + 10^{(a+bN_p)}\right)^{-1}$	Eq. (4-7)
2	Makszimov (1959)	$f_o = \left(1 + ba^{N_p} \ln a\right)^{-1}$	Eq. (4-8)
3	Craft-Hawkins (1959); Ershagi-Omoregie (1978)	$f_o = \left(1 + ae^{bS_w}\right)^{-1}$	Eq. (4-9)
4	Kazakov (1976)	$f_o = \frac{(1 - bN_p)^2}{(a - 2bN_p)(1 - bN_p) + bN_p(a - bN_p)}$	Eq. (4-10)
5	Gunkel Marsal-Philip (1968)	$f_o = \left(1 + a + (1 + cN_p)be^{cN_p}\right)^{-1}$	Eq. (4-11)
6	Gentil (2005)	$f_o(t) = \frac{1}{1 + F_{wo}} = \frac{1}{1 + \Delta W_i}$	Eq. (4-12)

CRM: Oil Fractional-Flow Model

$$q_o(t) = q(t) f_o(t)$$

$$f_o(t) = \frac{q_o(t)}{q_o(t) + q_w(t)} = \frac{1}{1 + \mathbf{WOR}(t)}$$

$$f_o(t) = \frac{1}{1 + a \left(\mathbf{CWI}(t) \right)^b}$$

$$\log \left(\frac{1}{f_o(t)} - 1 \right) = \log a + b \log \mathbf{CWI}(t)$$

A Method for Predicting the Performance of Unstable Miscible Displacement in Heterogeneous Media

E. J. KOVAL*

CALIFORNIA RESEARCH CORP.
LA HABRA, CALIF.

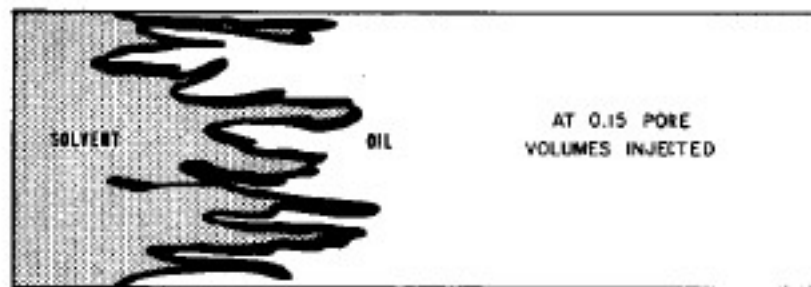
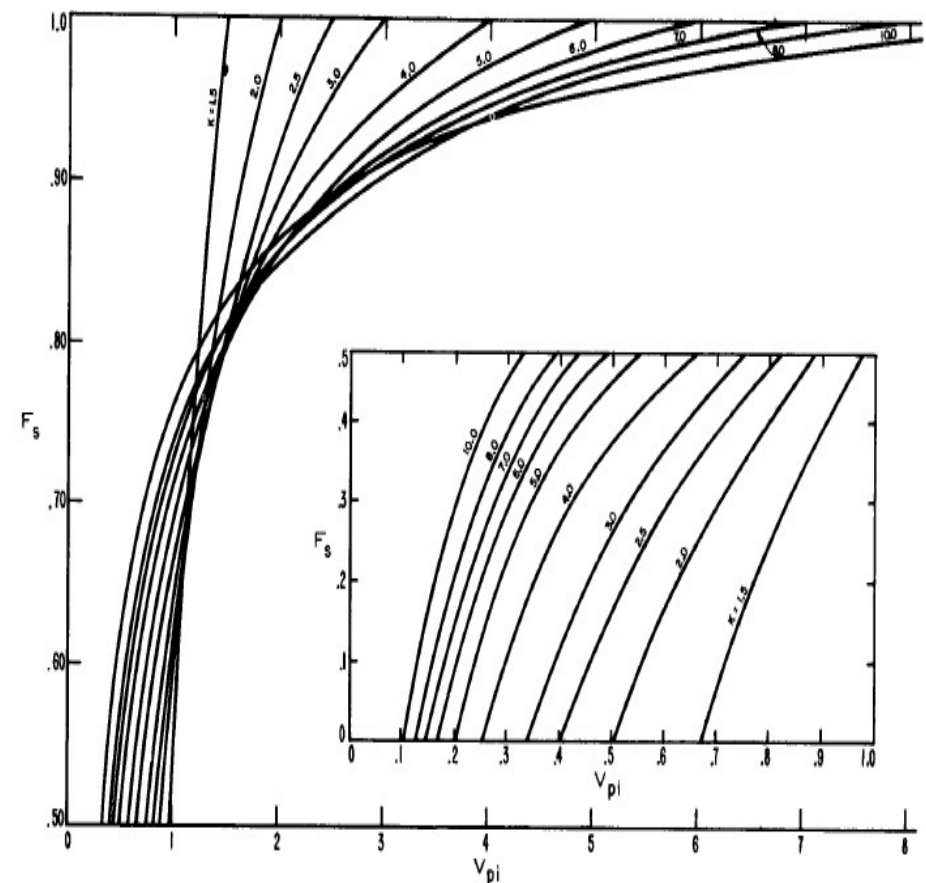
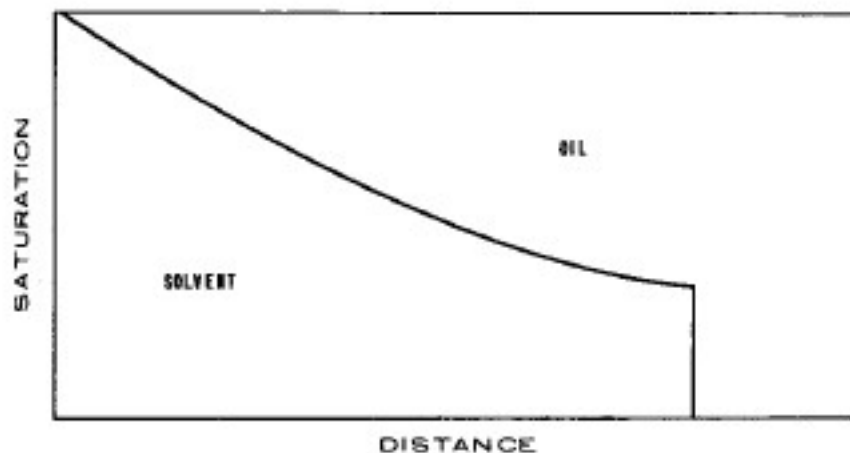


FIG. 4 — OBSERVED DISPLACEMENT FRONT FOR VISCOSITY RATIO OF 20 (AFTER BLACKWELL⁸).



Koval Model

A Method for Predicting the Performance of Unstable Miscible Displacement in Heterogeneous Media

E. J. KOVAL* | CALIFORNIA RESEARCH CORP.
LA HABRA, CALIF.

Koval model:

$$f_1 = \frac{1}{1 + \frac{(1 - C_1)}{K_v C_1}}$$

$$K_v = H_k E$$

H_k Heterogeneity factor

E = effective viscosity ratio

$H_k = 1$ (homogeneous)

$E = 1$ (tracer)

Basic Equations



Applications

- Effect of BHP
- Primary production
- CRM and tracers
- Oil rate modeling
- Optimization



Waterflood and EOR Optimization Work Flow

Workflow for Optimization

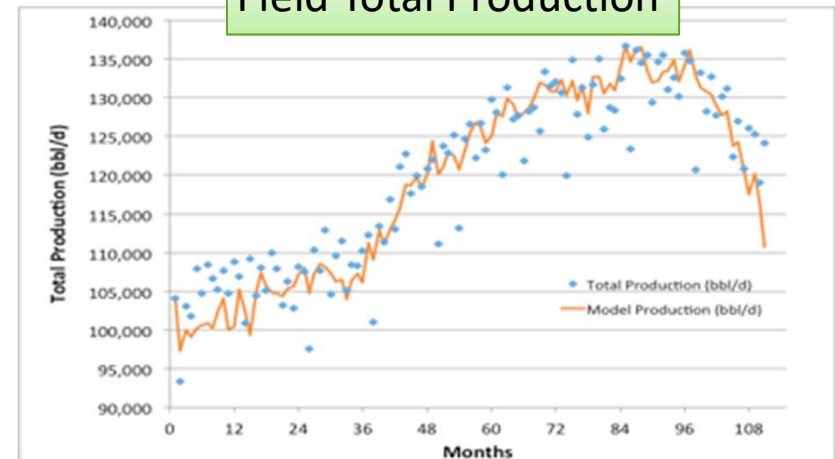
Fit CRM to total production data

Fit oil fractional flow model to oil production

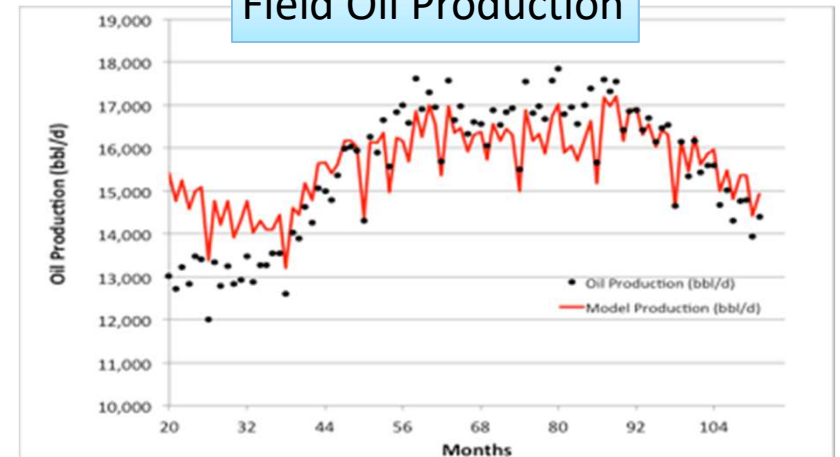
Use CRM and oil fractional flow model to optimize future injection and maximize NPV of future production

$$NPV = \sum_{j=1}^{n_p} \sum_{k=1}^{n_t} \frac{p_o q_{oj}(t_k; f_{ij}, \tau_j)}{(1 + D_f)^k} \Delta t - \sum_{i=1}^{n_i} \sum_{k=1}^{n_t} \frac{p_w}{(1 + D_f)^k} I_i(t_k) \Delta t$$

Field Total Production

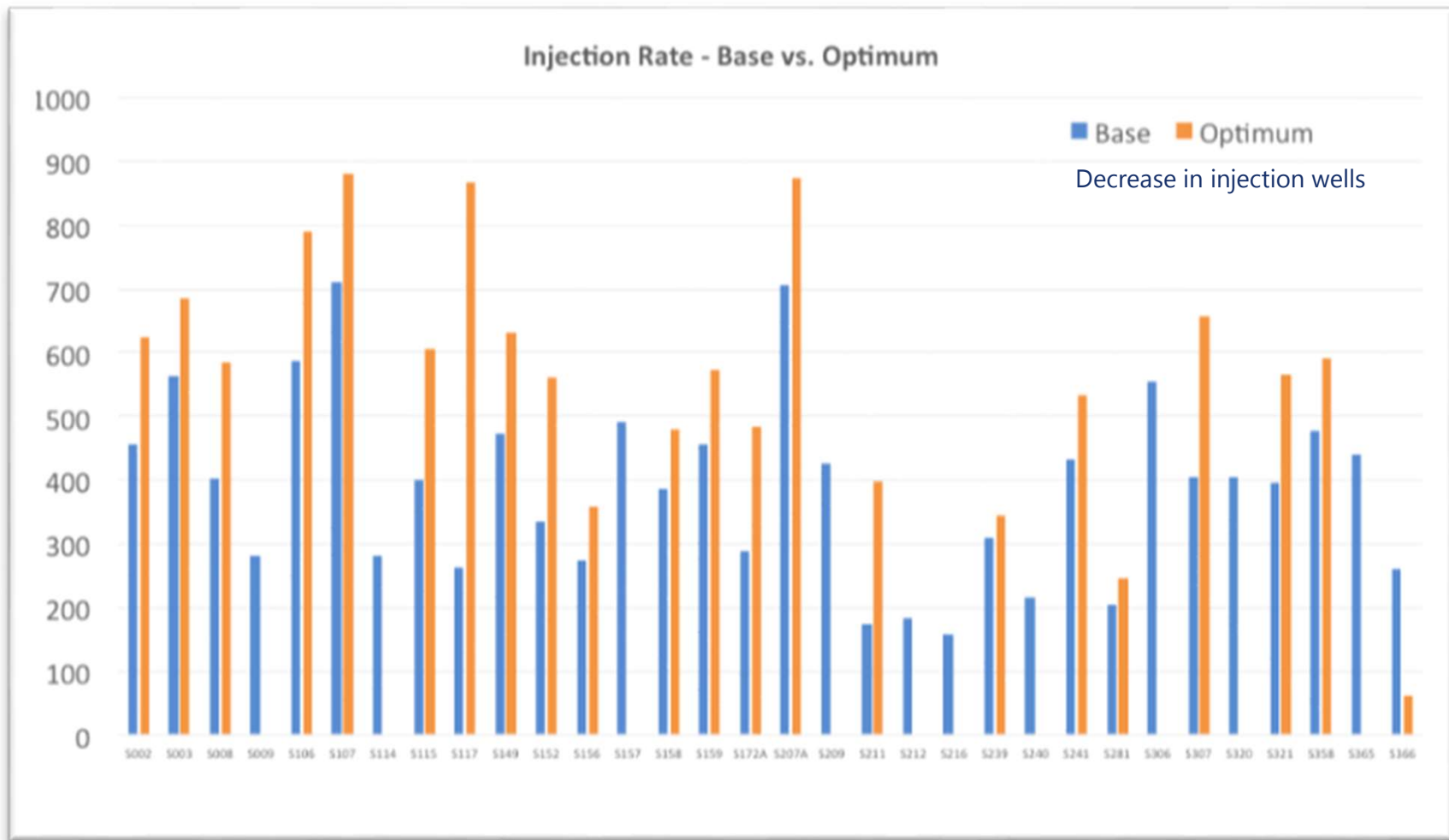


Field Oil Production



The Technology

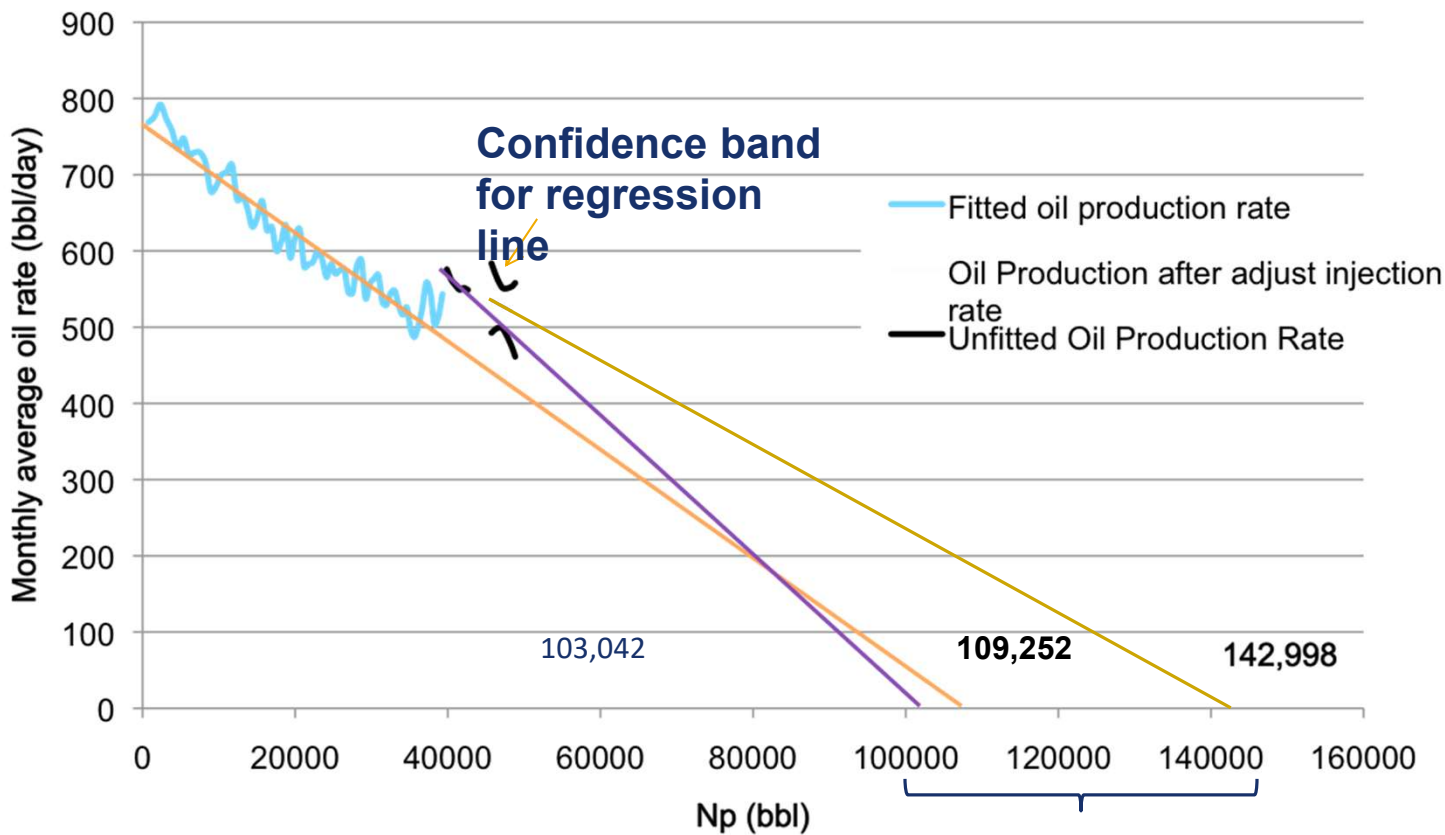
CRM Optimizes Operations





- Permian Study (Nguyen et al., 2012)
- Optimized oil production
- Modified only injection
- Reduced decline
- No additional capital costs

Rate vs. Cumulative Oil Production Oil



39,956 bbl
~ \$2,800,000

Basic Equations

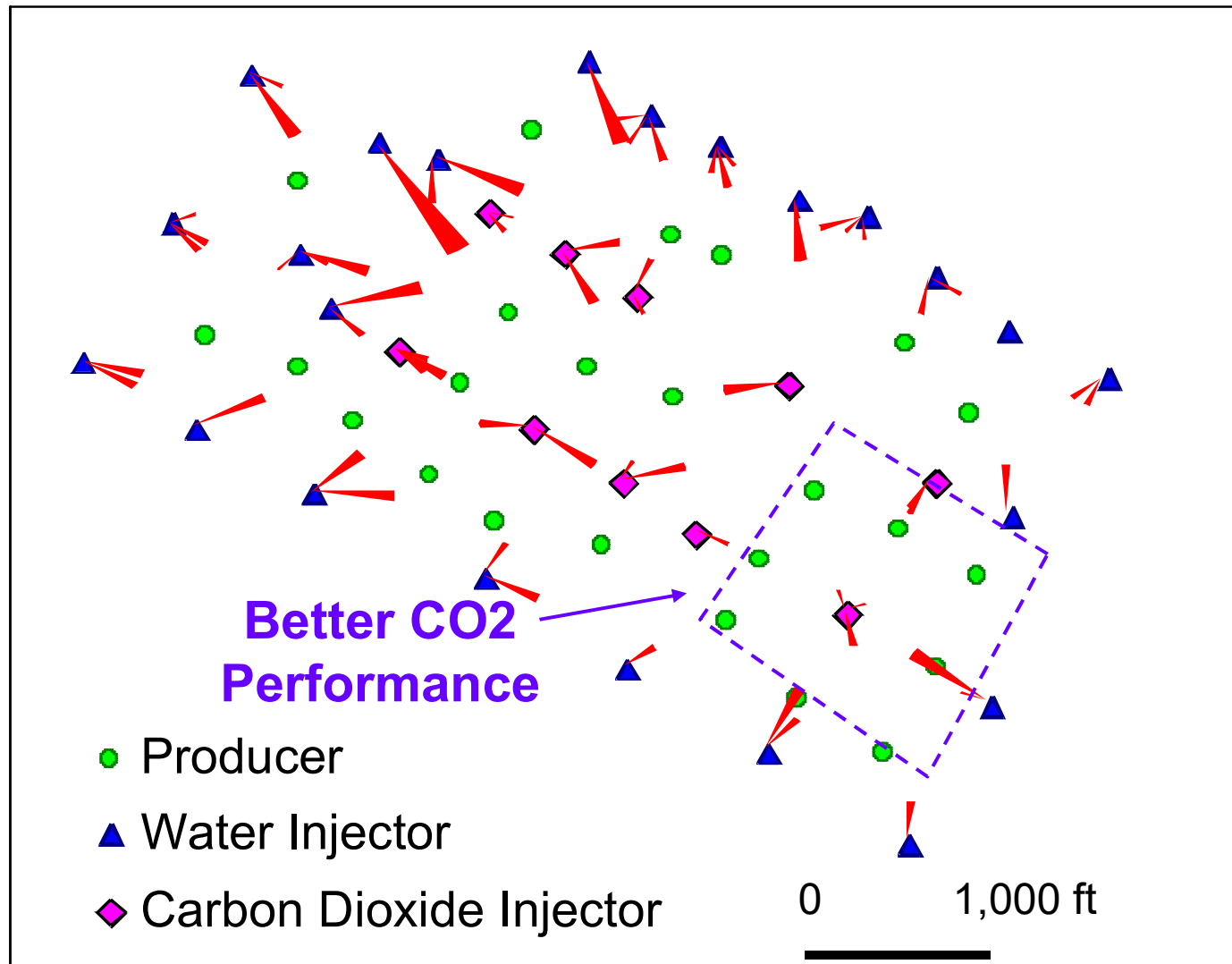


Applications

- Effect of BHP
- Primary production
- CRM and tracers
- Oil rate modeling
- Optimization
- Tracking CO₂ fronts

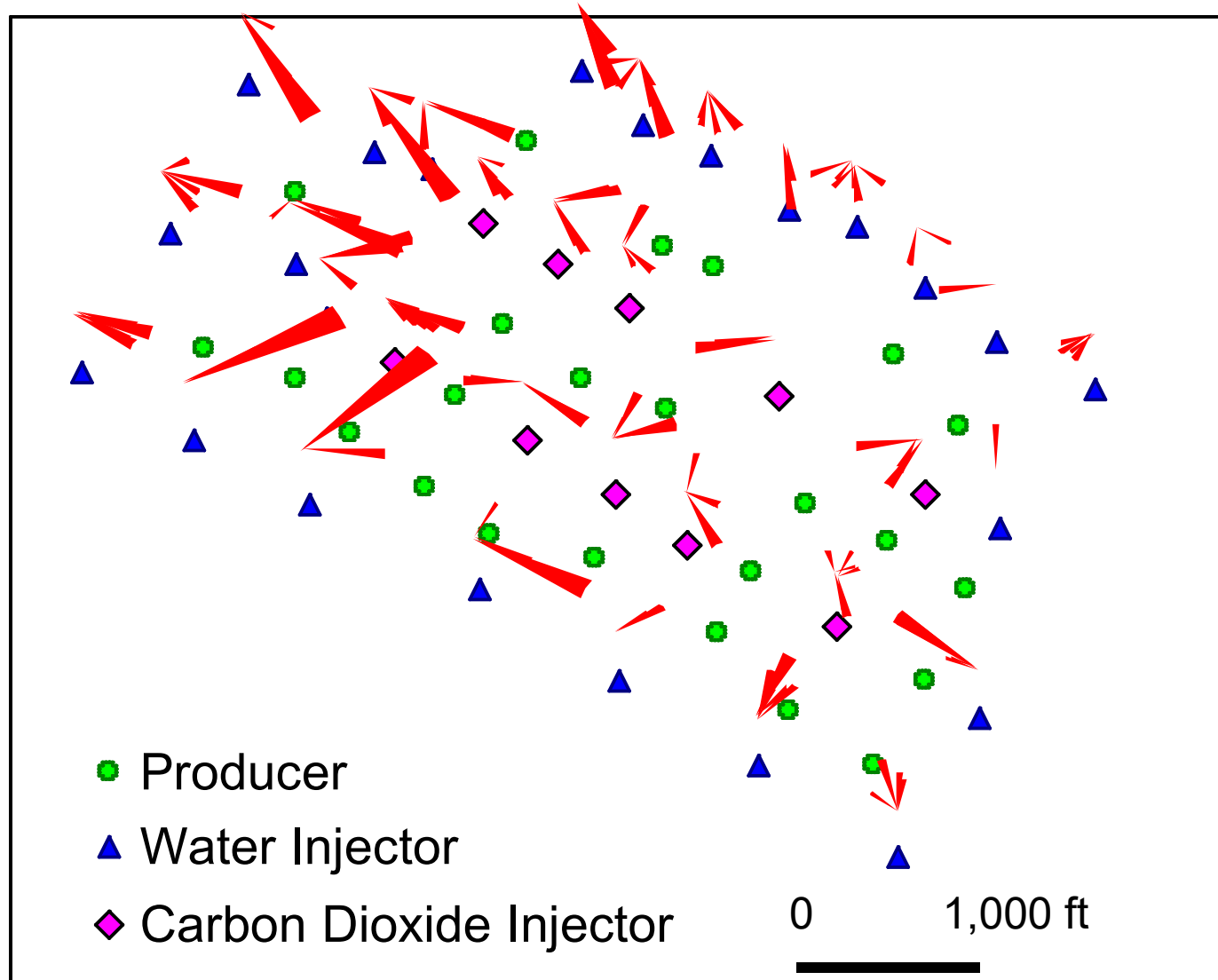


Steady-State Connectivity Map

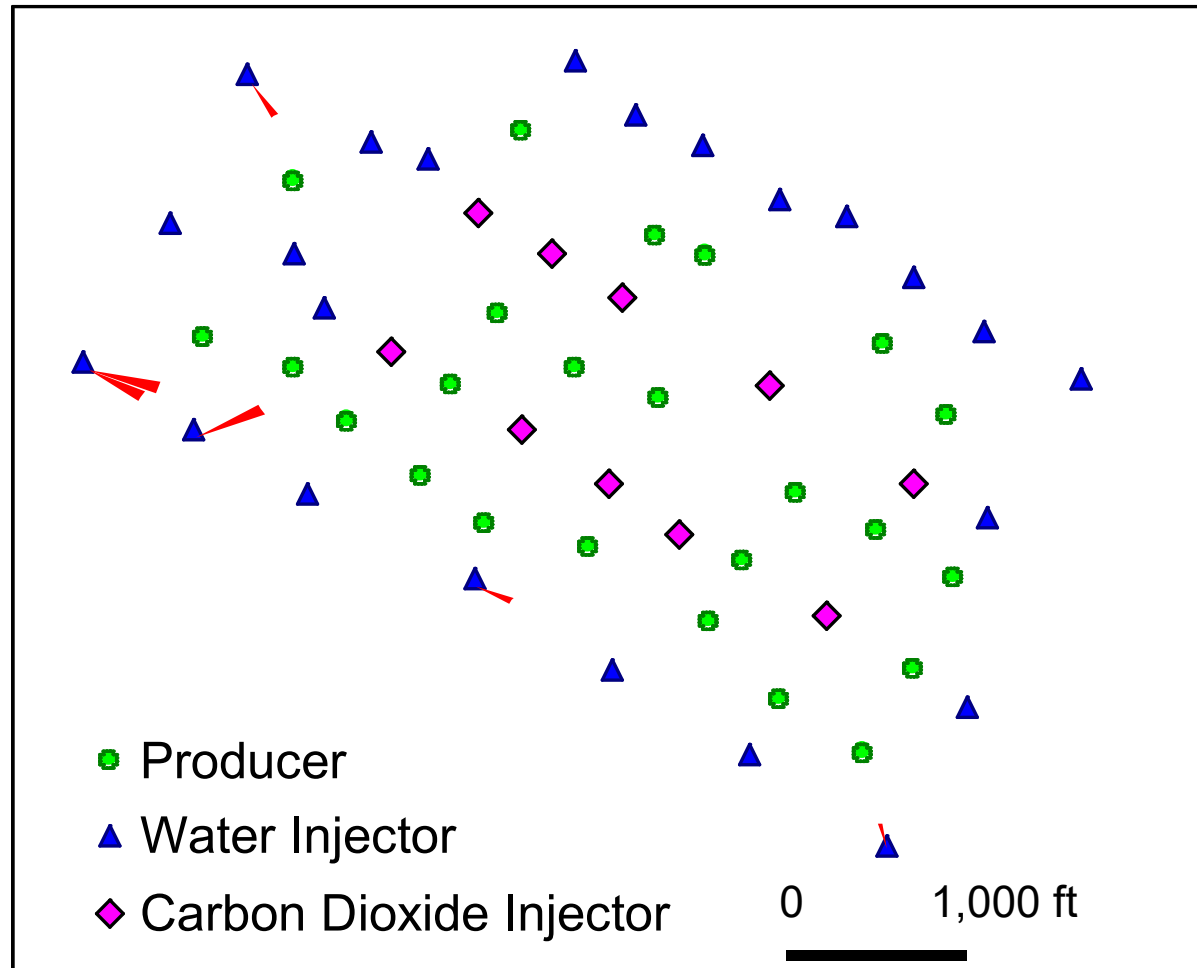


Interwell Connectivity

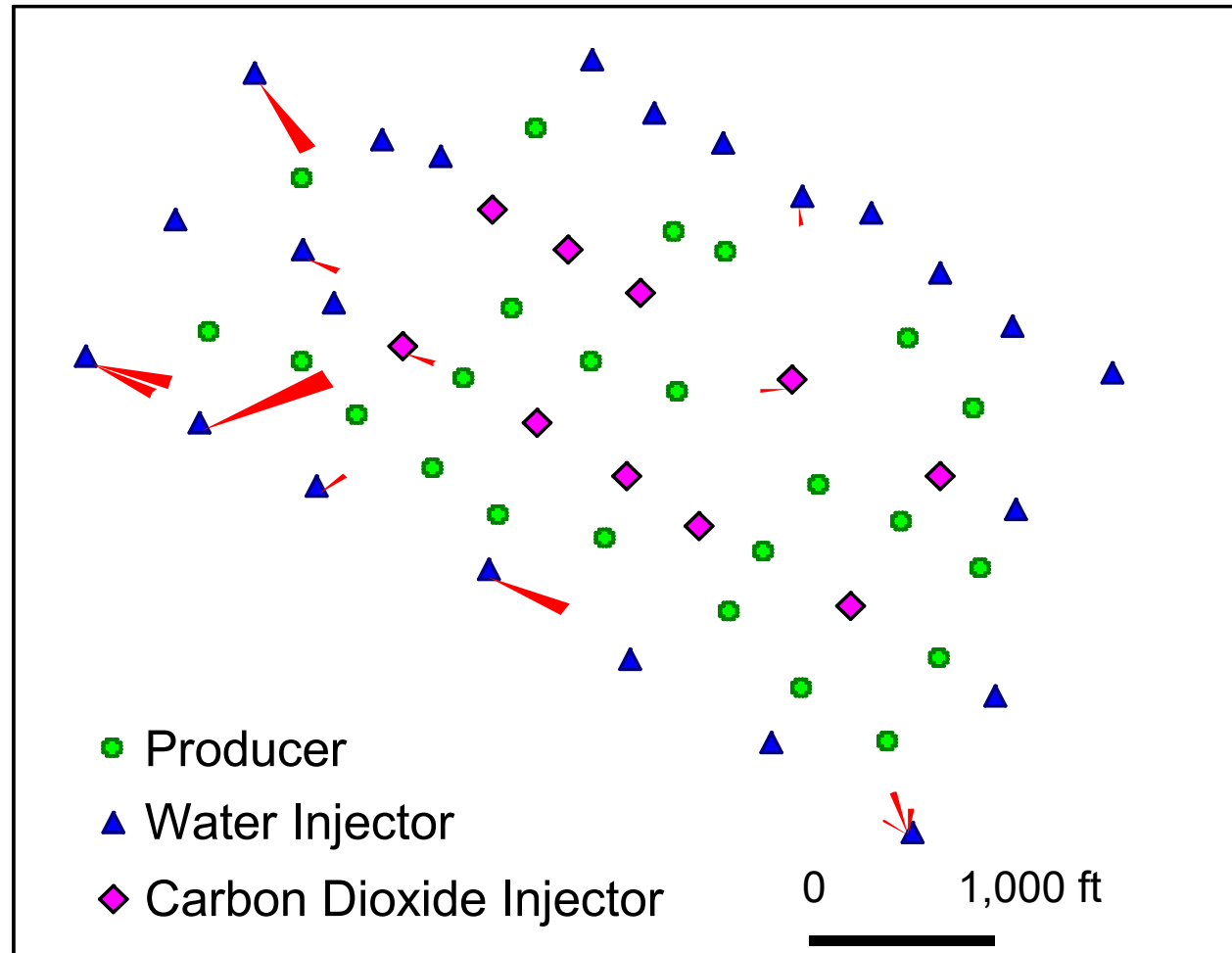
Two Equally Viable Solutions



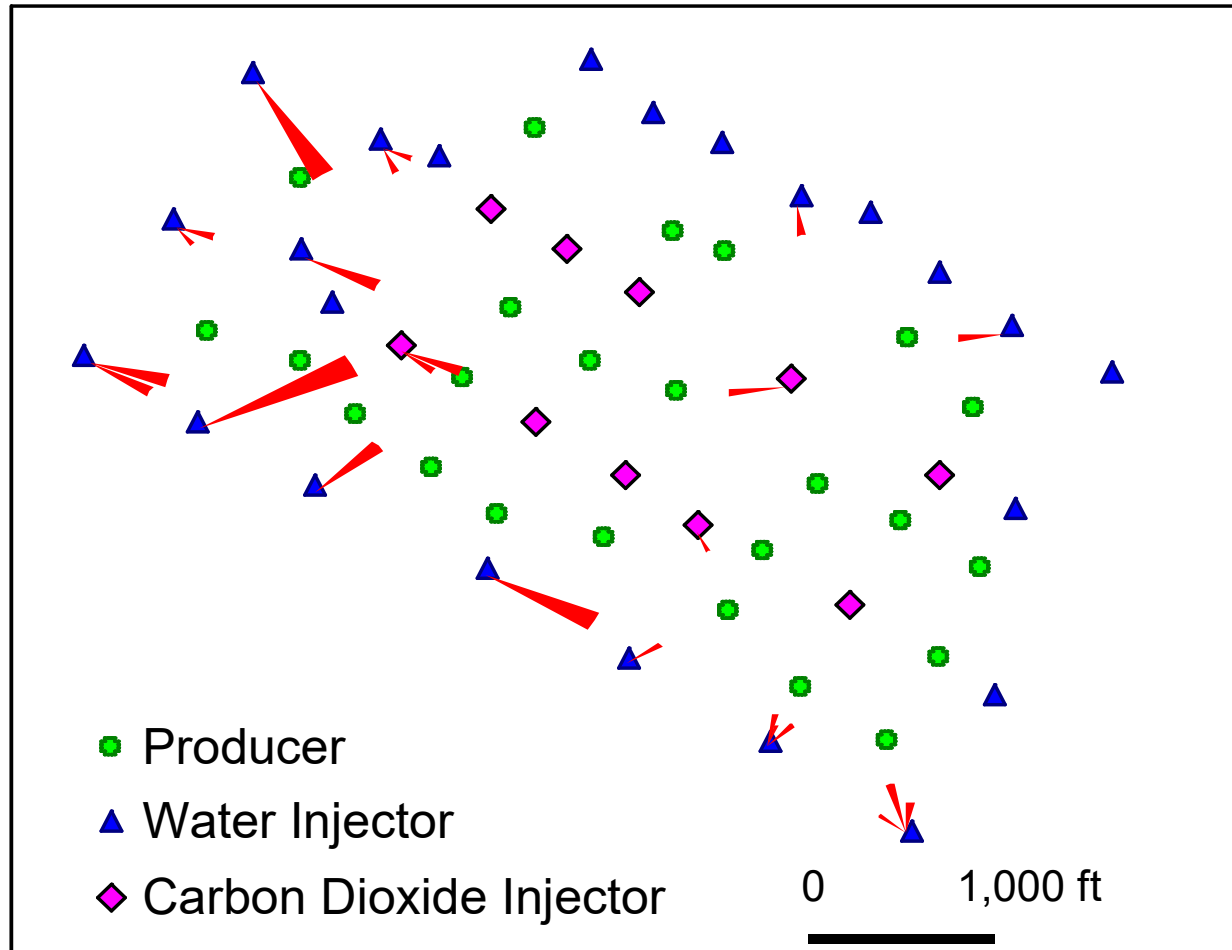
Transient Interwell Connectivity After 10 days



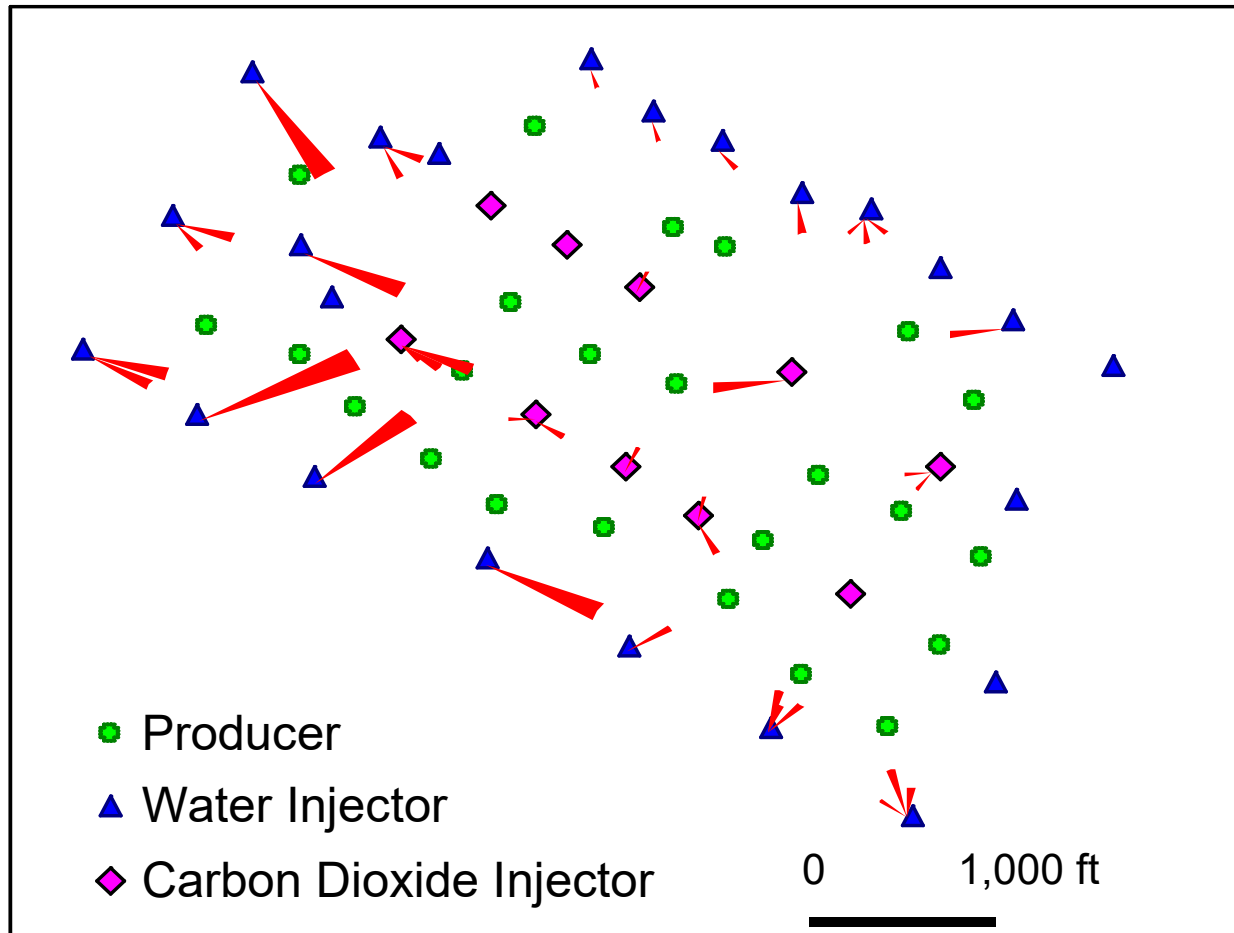
Transient Interwell Connectivity After 30 days



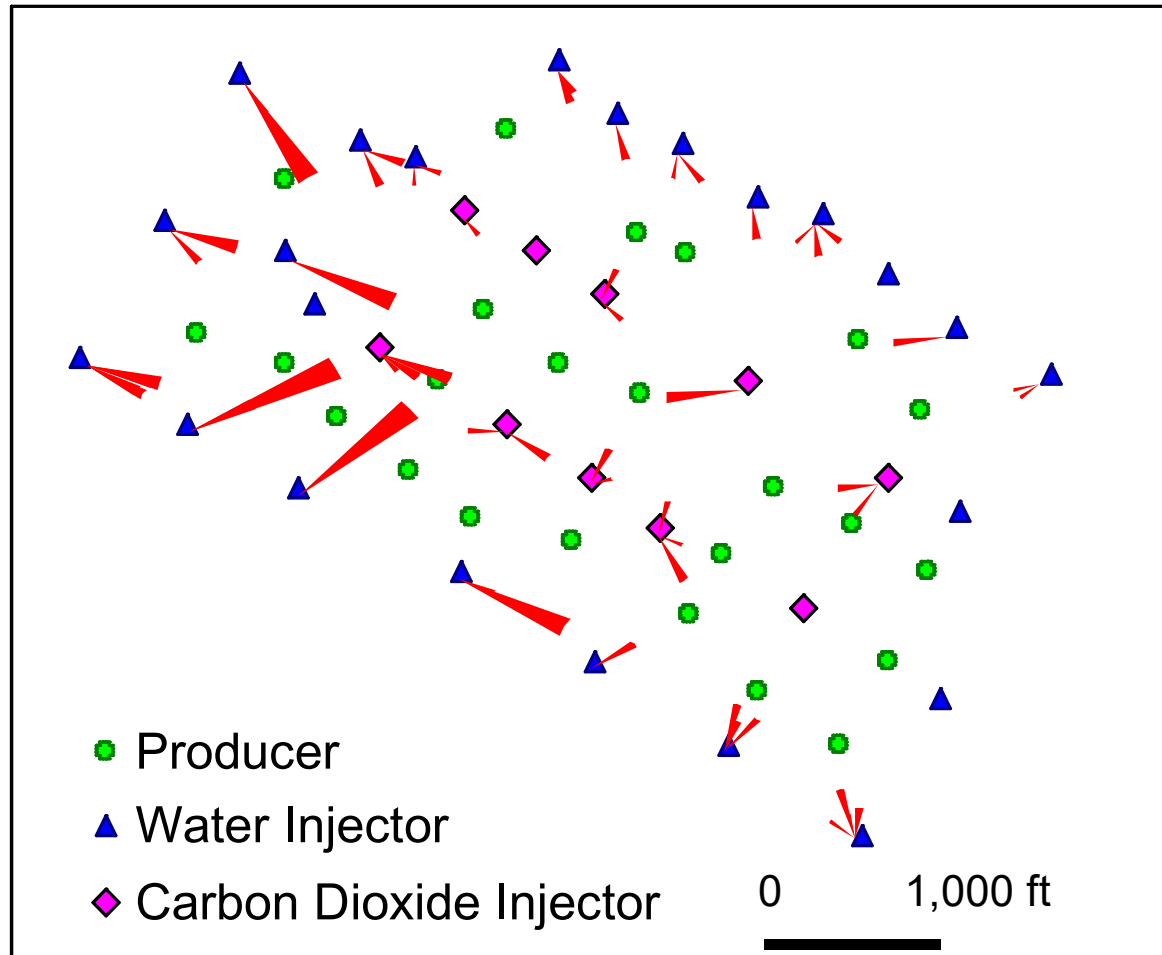
Transient Interwell Connectivity After 90 days



Transient Interwell Connectivity After 180 days



Transient Interwell Connectivity After 365 days



Basic Equations



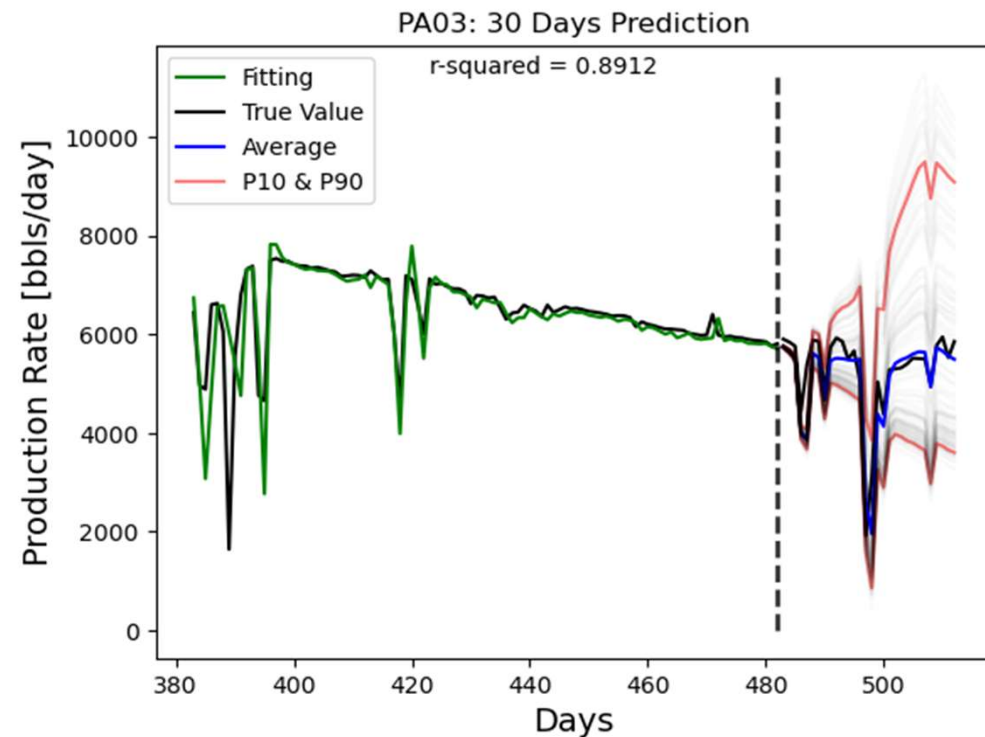
Applications

- Effect of BHP
- Primary production
- CRM and tracers
- Flow capacity curves
- Oil rate modeling
- Optimization
- Tracking CO₂ front
- CRM and machine learning



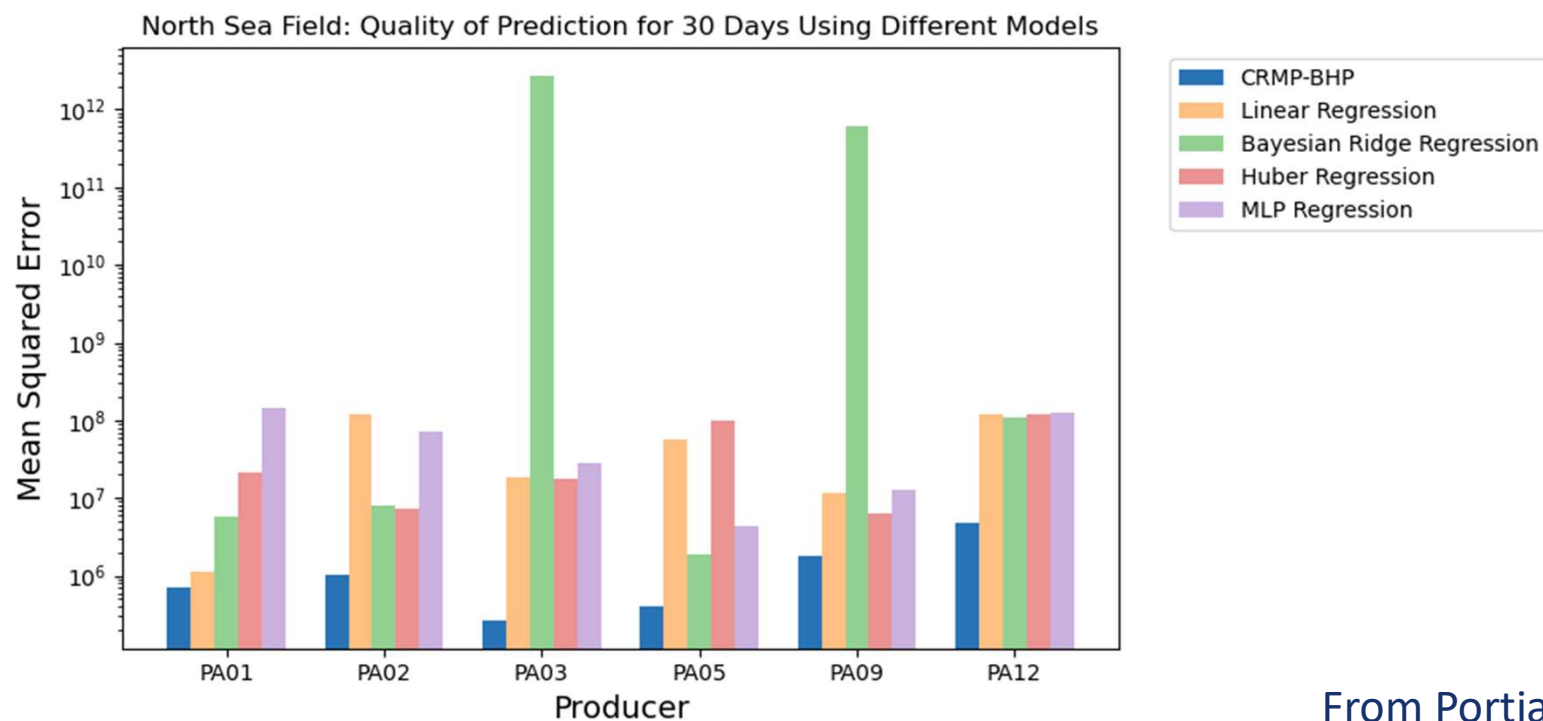
Ensemble Bootstrapping Prediction Distribution Using CRMP with Bottomhole Pressure (BHP)

- 100 Bootstrap realizations
- Goodness Measure: 0.9030
- MSE: 260,772



From Portia and Foster

Converged Errors of Models for North Sea Field Example



From Portia and Foster

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