



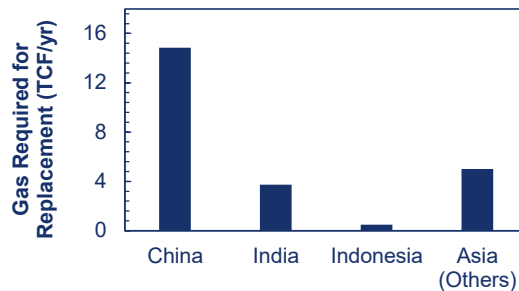
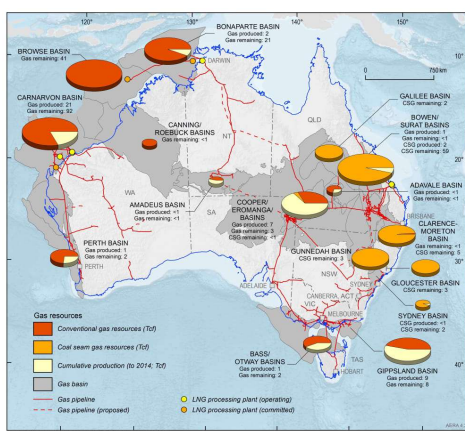
Hydrate Risk Management Informed by High-Pressure Laboratory Experiments

Prof. Zach Aman
3 April 2023





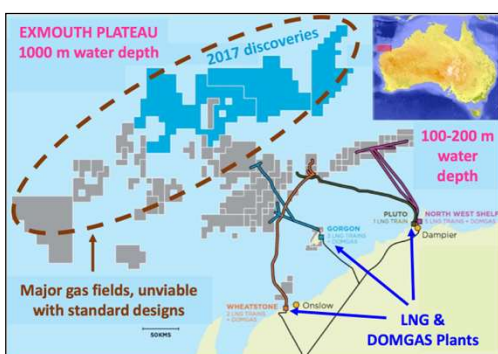
Context of Large, Remote Australian Fields



- **Regional coal-to-gas switching**
 - **India:** 40 years of supply, saving 500 Mt CO₂ per year; or
 - **Asia (w/o China):** 30 years of supply, saving 800 Mt CO₂ per year
- **Including prospective resources**
 - Enough to supply **all** of China, India, and remaining Asia for **15 years**
 - Saving **3.5 Gt CO₂ per year**



Australia's Focus on Long Tiebacks



Gas transport of 100 to 300 km

- 3× definition of “long” from N. America

99 tcf of economic gas in Australia

- 57 tcf of sub-economic (2012)
- Sub-economic:
18 tcf Browse,
22 tcf Carnarvon,
13 tcf Bonaparte



World LNG Report (2018)

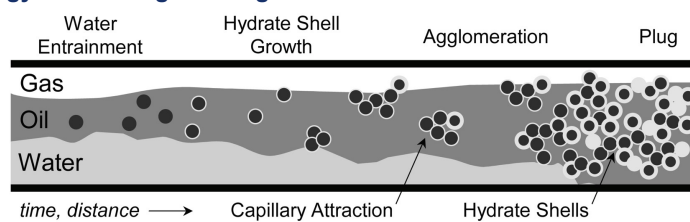


Requirement for
cost effective
solutions

Hydrate Constraint in Oil-Dominant Flow

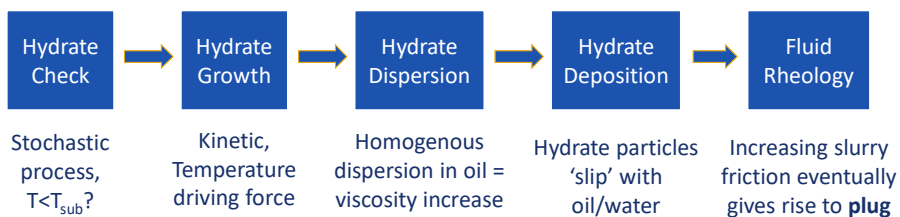


Phenomenology of Evolving Blockage



(E.D. Sloan et. al – Natural Gas Hydrates in Flow Assurance, 2011)

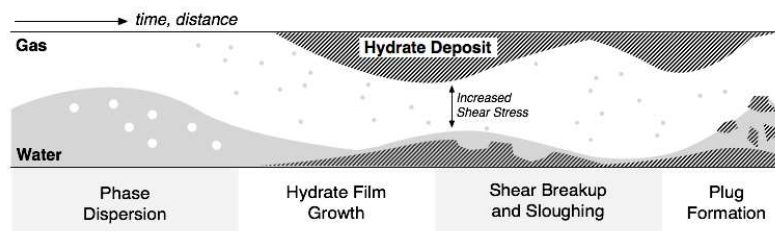
Model Representation in Transient Simulator



Hydrate Constraint in Gas-Dominant Flow

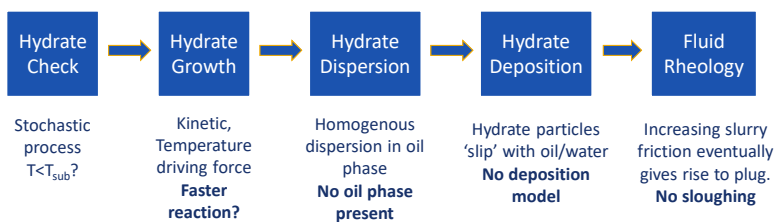


Phenomenology of Evolving Blockage



Model Representation in Transient Simulator

(based on M.N. Lingelem et al. 1994)



Pilot-Scale Systems to Understand Gas-Dominant Hydrate Phenomena



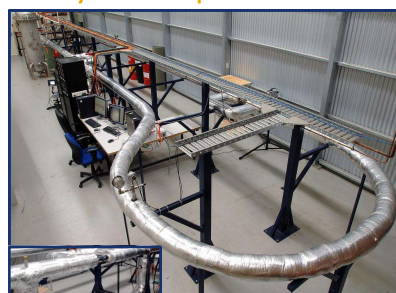
- Simulate deep-water gas field conditions
- Liquid loading below 10 vol%
- High gas velocity, wavy-annular flow regimes
- Constant-flow and transient-flow tests

TECHNICAL SPECIFICATIONS

Test section	1 inch SS 360 pipe, 40 m long Pipe-in-pipe temperature control
Conditions	Pressure: <1750 psi (120 bar) Temperature: -8 to 30 °C
Fluids	Aqueous solutions, light oils, natural gas
Flow rates	Liquid: 1-8 Litres/min V_{SL} : 0.05-0.4 m/s Gas: 500 - 1000 scfm V_{SG} : 4.5-8.2 m/s
Instruments	7 pressure transducers, 7 RTD sensors, gas and liquid flow meters, viewing windows, high speed camera



Hytra flowloop test section



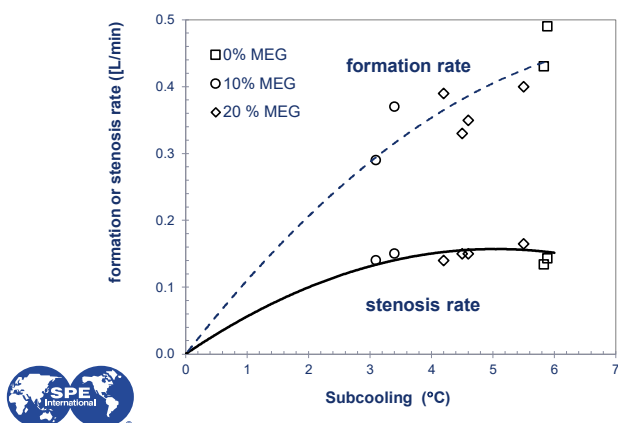
U-bend section



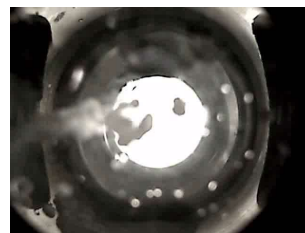
Stenosis and Sloughing in Gas Lines



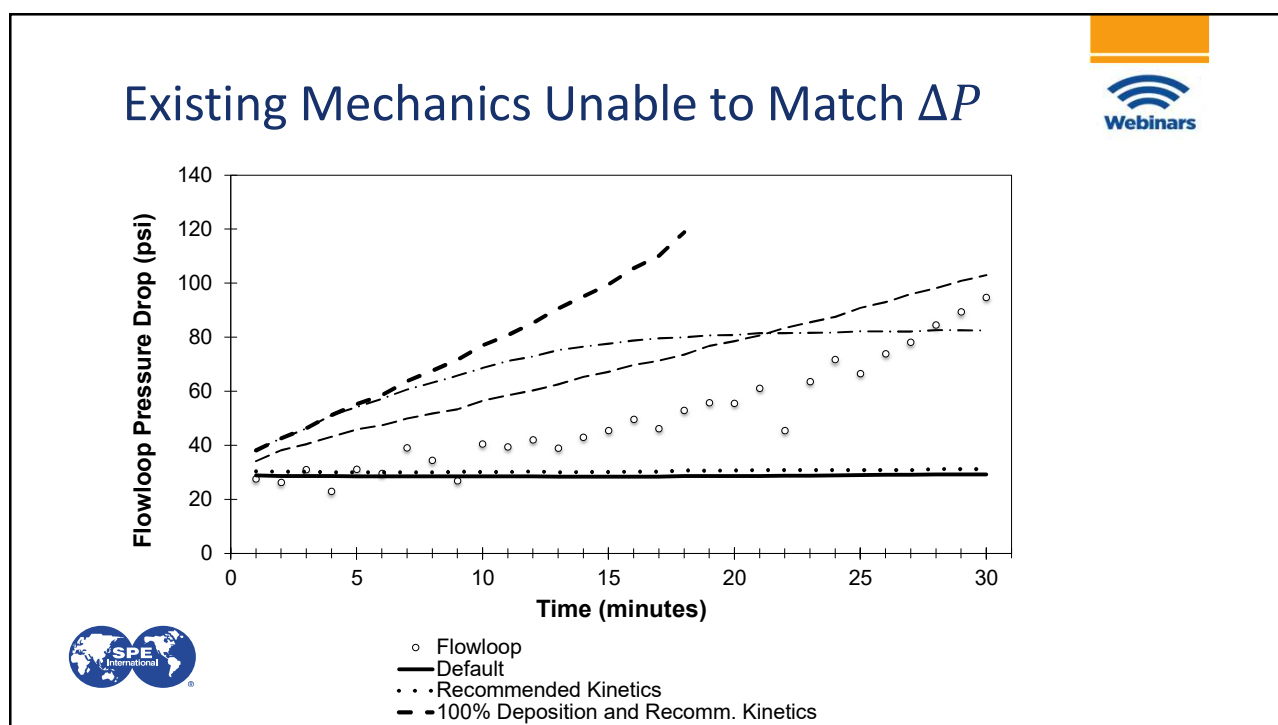
- Flowloop investigation of hydrate formation and stenosis

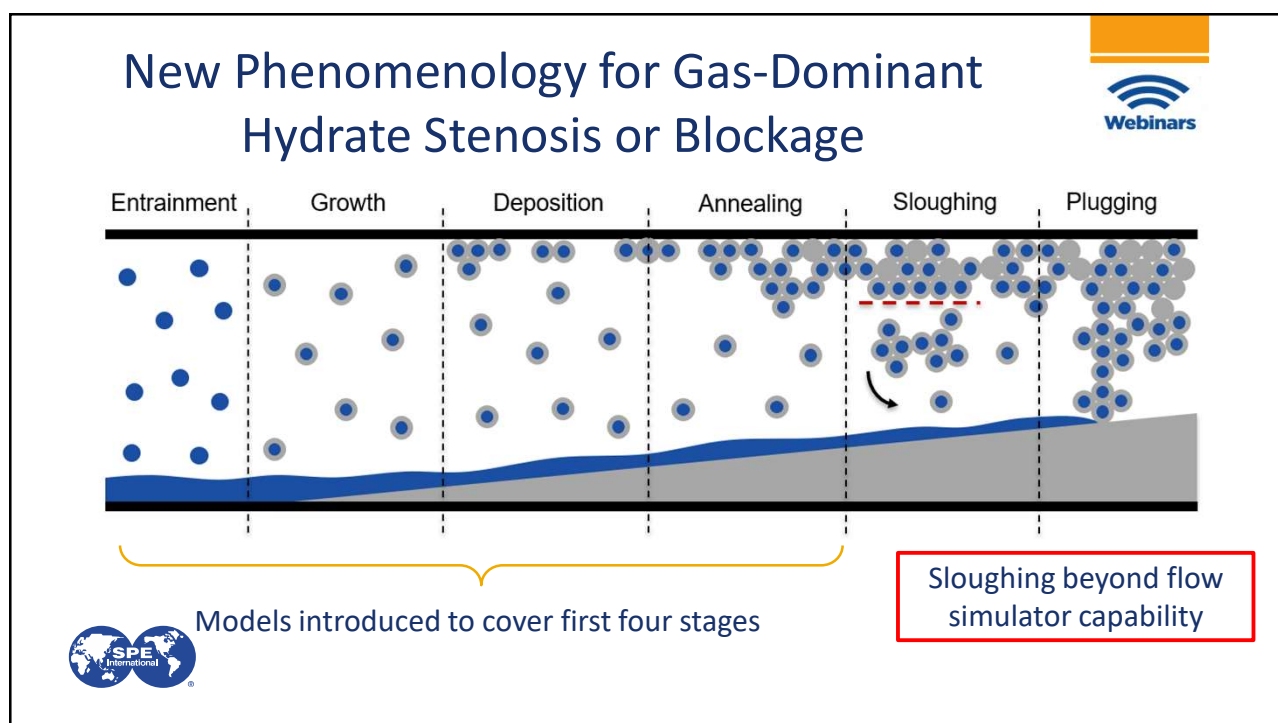


Formation rate
30-50% larger
than stenosis in a
subcooling range
of 3-6 °C



(1) Di Lorenzo, M. et al. *Energy Fuels*, 2014, 28 (11), 7274–7284

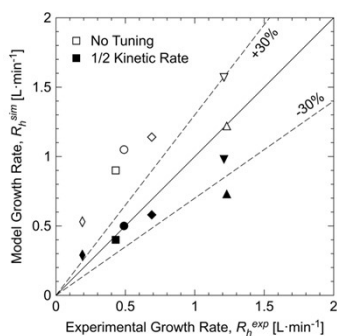




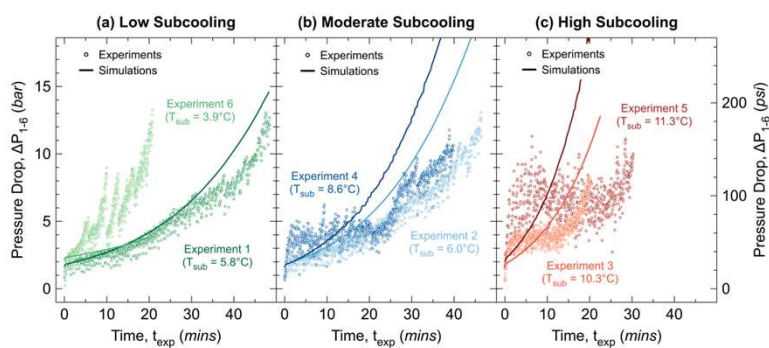
Early Comparison with Flowloop Data



Growth



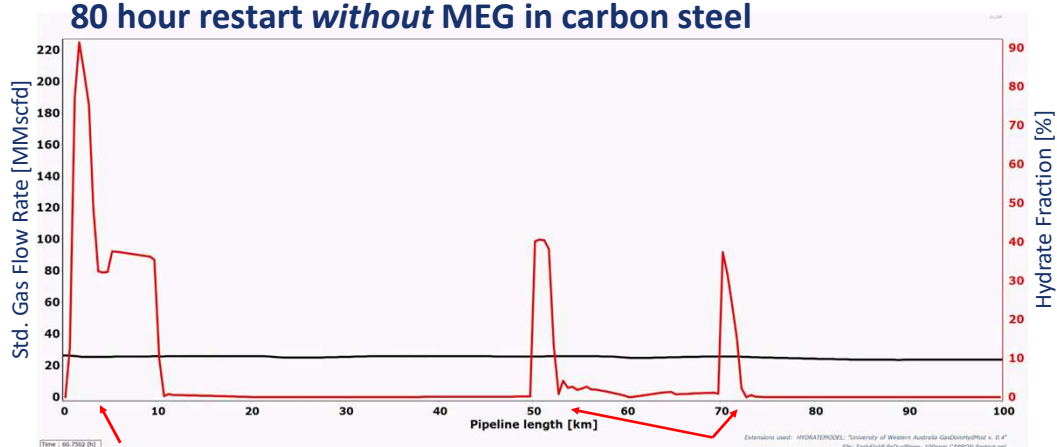
Deposition (without tuning)



Example: Blockage in Uninhibited System



80 hour restart *without* MEG in carbon steel



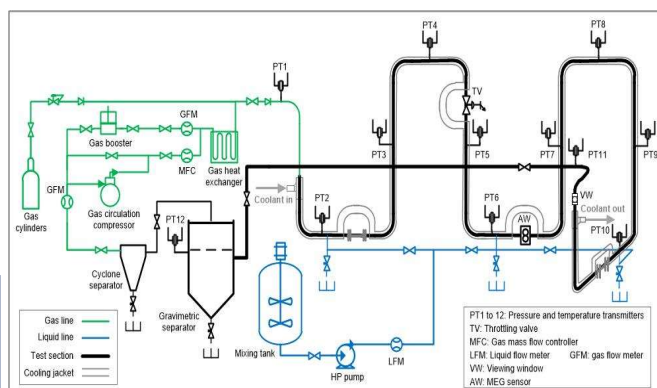
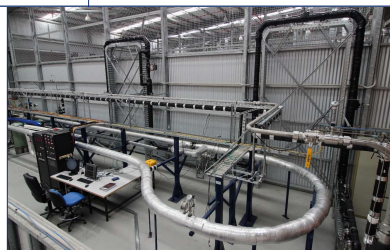
Severe deposit in < 8 hrs

Secondary
deposits at $\approx$ 18
hrs

Expanding to Jumper and JT Loops

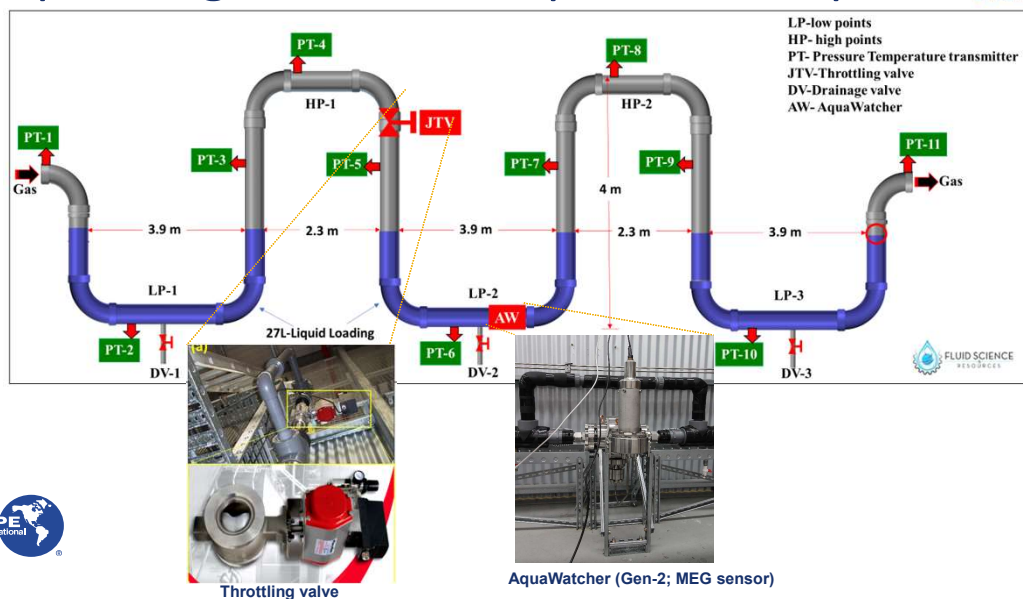


TECHNICAL SPECIFICATIONS	
Geometry	2 inch OD SS 360 pipe 2 high points, height: 4 m 3 low points Total length: 35 m Cooling jacket
Conditions	P: <120 bar (1700 psi) T: -4 to 30 °C
Gas velocity	V_{SG} : 0.02 to 2 m/s
Instruments	11 Pressure, RTD sensors Gas flow meter, MEG sensor
Test section volume	51.4 L



HyJump (black) and Hytra (silver) flowloop test sections

Expanding Effort to Jumper Flowloop

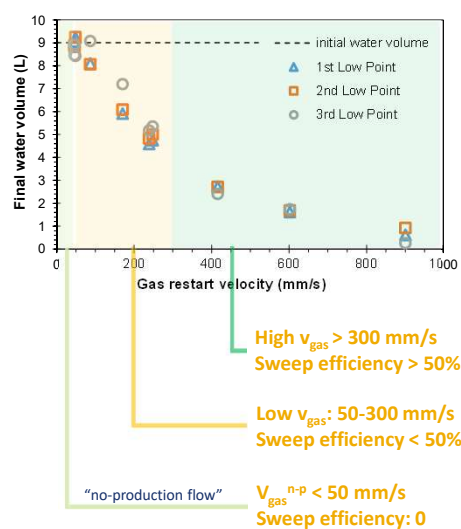
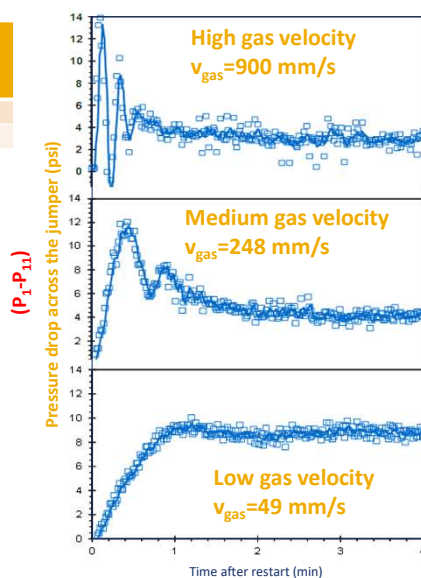


Sweep Efficiency on Restart (Jumper)

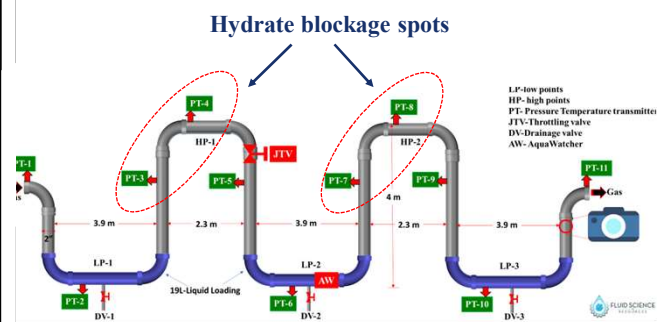
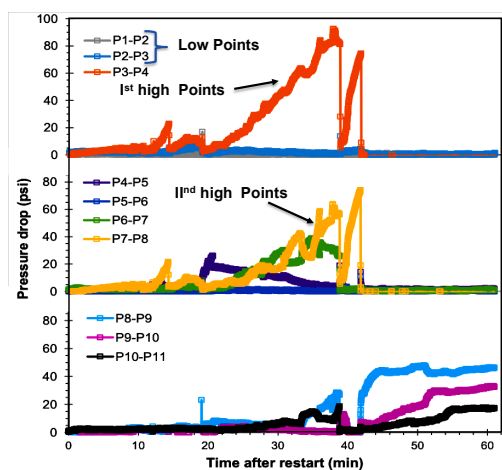


Shut-in pressure	Shut-in temperature
(psi)	(°C)
1189	17.8

No hydrates in the system



Accumulation in Bends, High Points



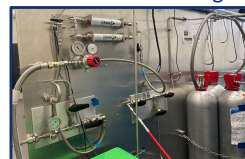
Incorporating a Dedicated JT Loop



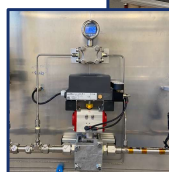
Post-experiment
gas storage



Moisture removal stage



Gas
compressor

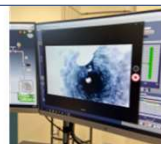


Controllable JT Valve

Detachable test section (0.83" I.D.)



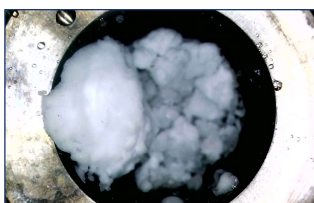
Post-experiment visual observation



Rapid Plug Onset in Severe JT Expansion



Test section inlet

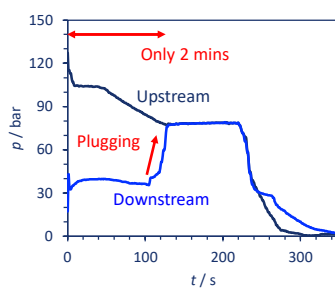
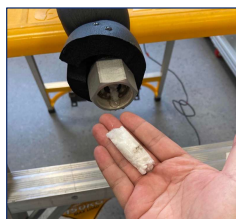


Test section outlet



Variables affecting Hydrate formation

- *Pressure drop*
- *Fluid temperature*
- *Water droplet size (entrainment)*
- *Working fluid*



CH₄ + Water

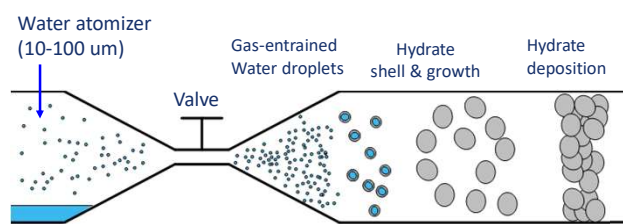
$P_{\text{feed}} = 115 \text{ bar}$, $T_{\text{feed}} = 8^\circ\text{C}$

Back Pressure regulator = 30 bar

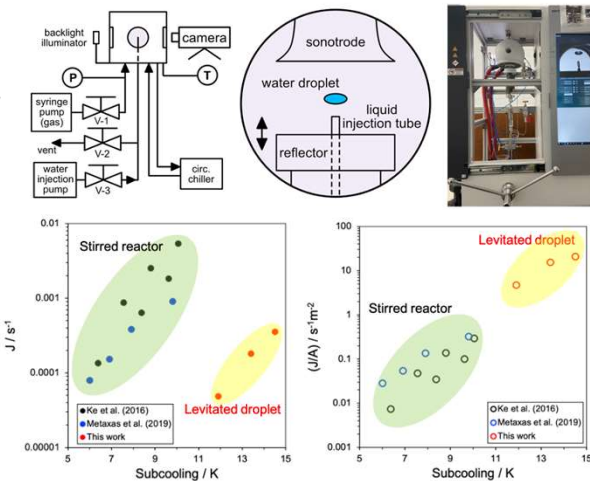
Total water loading = 533 ml



Entrained Surface Area Dominates Growth



500 μm

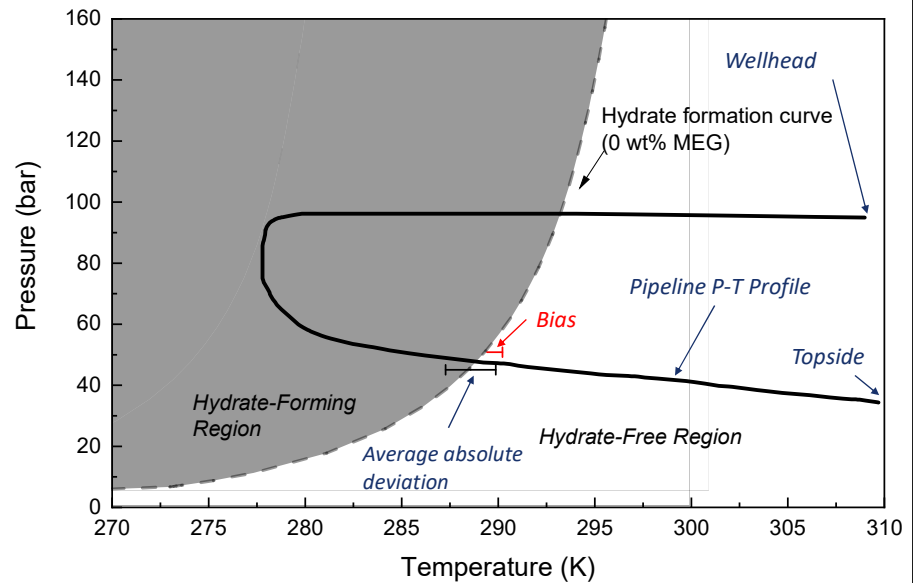


- Total interfacial area of atomized water droplet is **4 orders of magnitude larger** than bulk water

Uncertainty is the Key to Cost



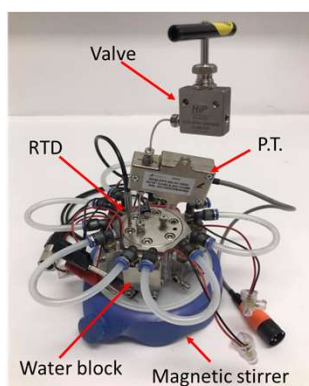
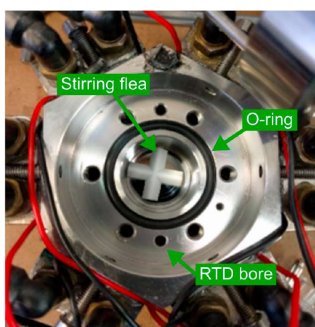
- **Bias** highlights conservativeness of hydrate model prediction
- Uncertainty bounds change with **system fluid composition**
- **Paucity of data >50 wt% MEG** → larger uncertainty (as shown)



Establishing Nucleation Probability



Stirred system
Small thermal mass (11 mL)

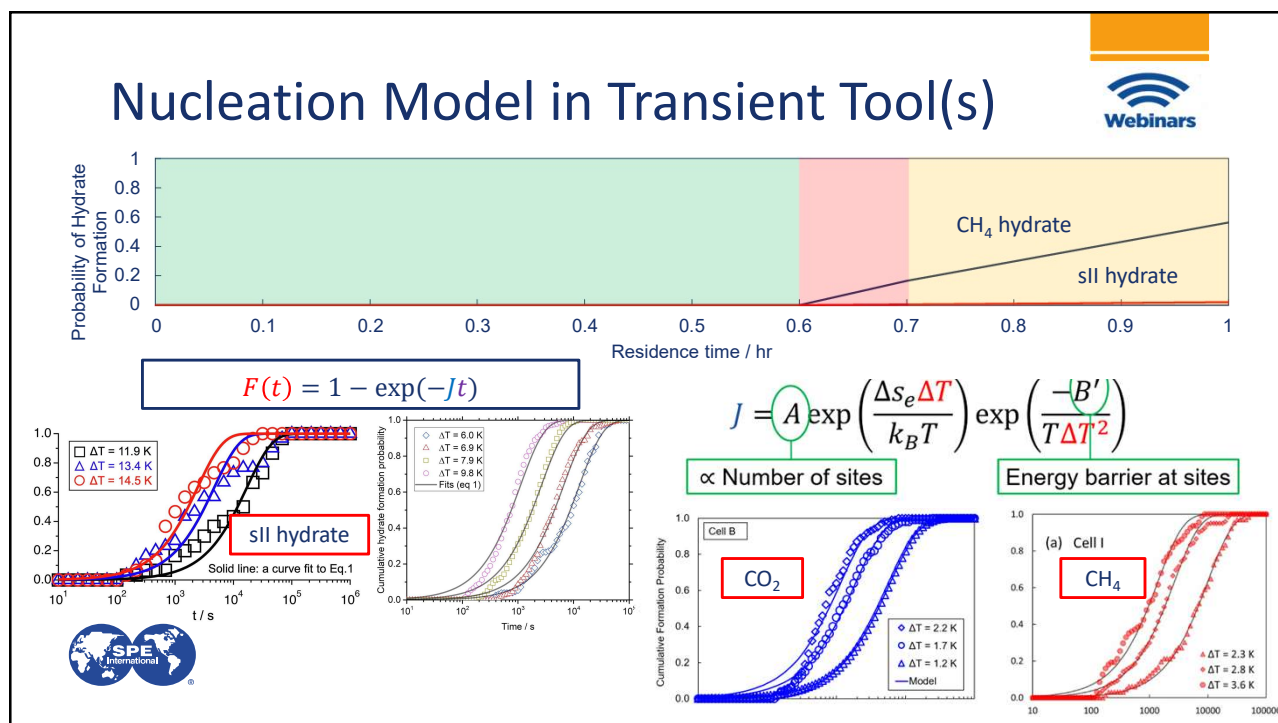


Peltier driven cooling system
(up to 5 K/min)

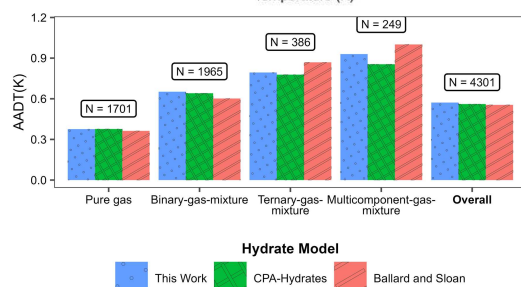
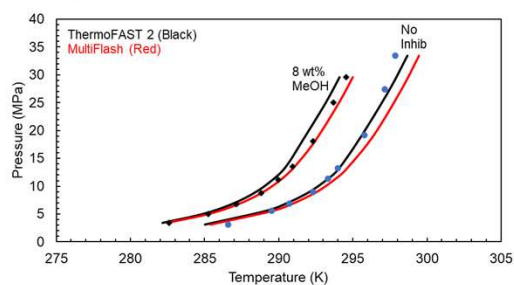
Thermal enclosure for
ambient temperature control



Metaxas, Lim et. al., *Fuel*, 252, 448-457, 2019
Lim et. al., *CEJ*, 124177, 2020



A New Hydrate Phase Boundary Model



Hydrate Equilibrium Model	Parameters
Ballard and Sloan (2002)	103
Hielscher et al. (2019)	92
Zhu et al. (2022) – THIS WORK	64

Component	Mole Fraction
CO ₂	0.0134
Methane	0.7724
Ethane	0.0761
Propane	0.0369
Isobutane	0.0056
N-butane	0.014
Isopentane	0.0003
N-pentane	0.0089
Hexanes	0.0067
C ₇₊	0.0657

Summary



- Pilot-scale flowloop systems to establish phenomenology
 - Hytra (horizontal) system: entrainment > subcooling
 - HyJump (jumper-based) system: bends, high points
 - JT expansion loop: entrained droplet size, pressure drop
- Interfacial efforts to improve transient model prediction
 - HP levitation and HPS-ALTA: establishing nucleation probability
 - Phase boundary, integrated compositional tracking

