



Can Formation Testing Time be Cut in Half and Generate Ten Times the Data?



Mark Proett Consulting LLC
June 2, 2022



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Mark Proett - Profile



- Petroleum engineering consultant with over 40 years experience (Aramco, Halliburton & Schlumberger).
- Known for publications advocating automated testing methods, focused sampling and the viability of formation testing-while-drilling (FTWD).
- 80 US patents and more than 60 technical papers, most of which deal with sampling and testing methods.
- Numerous Industry Awards including:
 - SPWLA Distinguished Speaker (twice) and SPE Distinguished Lecturer (twice)
 - 2008 SPWLA Distinguished Technical Achievement Award
 - 2013 SPE Gulf Coast Regional Formation Evaluation Award
 - 2017 the SPE International Formation Evaluation Award
- BSME from the University of Maryland and a MS Johns Hopkins University



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Overview

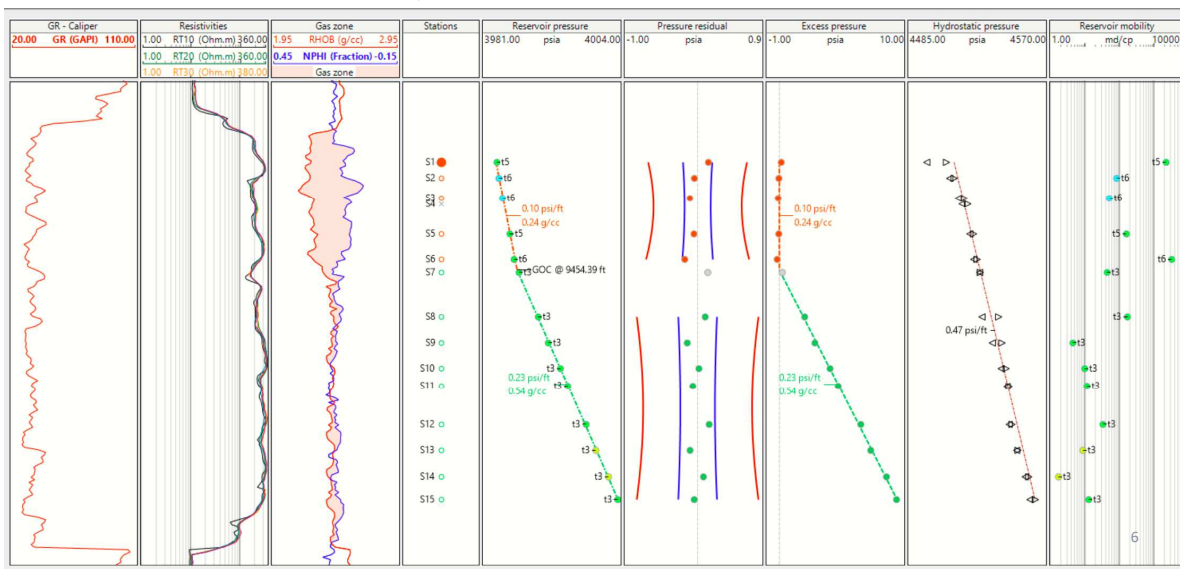


- The trouble with pretests
- Interval Pressure Transient Testing (IPTT - MiniDST)
- What is needed k_h , S , k_v/k_h , h for every pretest
- Probe geometry anisotropy dependency
- Probes and heterogeneities (dip & azimuth)
- New probe designs can resolve heterogeneities
- Concluding remarks

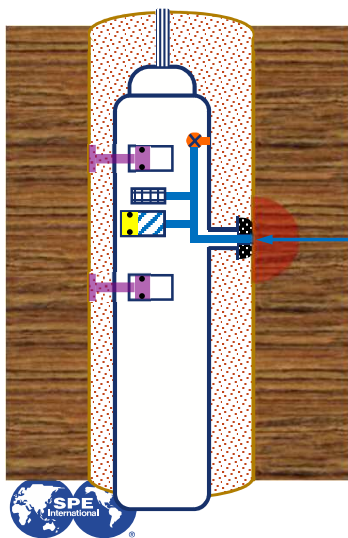


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Typical Pretest Pressure Survey (Courtesy KAPPA-Azurite)



Formation Tester Pretest (5-15 min typ.)



Process is automated by software providers

Q (cc/sec)

Quality of Test Data

P (psia)

P_f Final Buildup Pressure

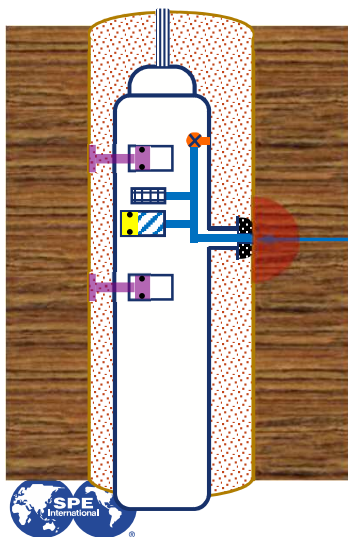
$$M_s = C_{pf} \frac{Q}{\Delta P_{dd}}$$

Spherical Mobility (md/cp)

Mark Proett, et al., SPWLA 2014

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The Trouble with Pretests



$$M_s = C_{pf}(\lambda) \frac{Q}{\Delta P_{dd}}$$

$$M_s = (1 + S) C_{pf}(\lambda) \frac{Q}{\Delta P_{dd}}$$

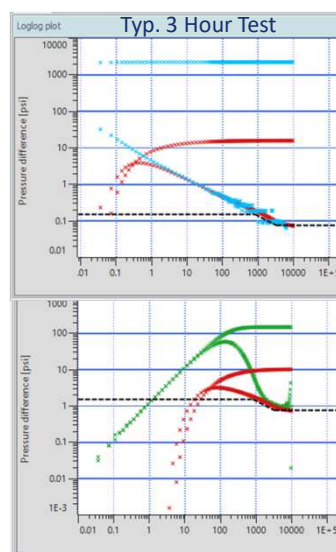
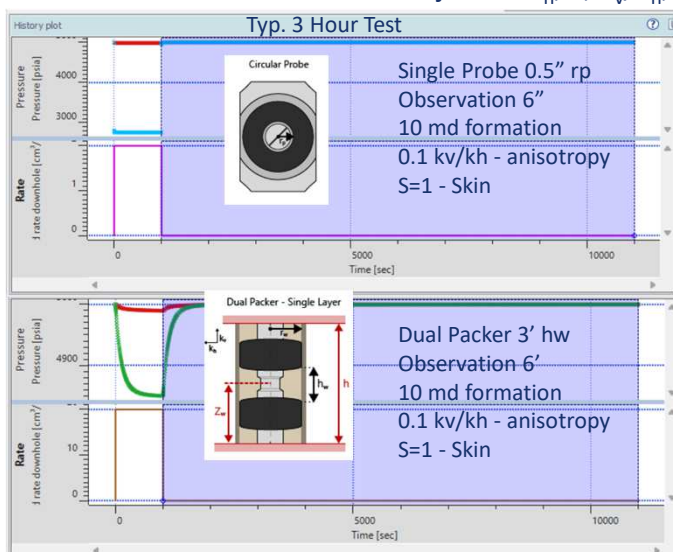
- Coefficient $C_{pf}(\lambda, \theta_d \text{ \& } \theta_a)$
 - λ – anisotropy
 - θ_d – bedding dip
 - θ_a – azimuth
- Skin – Wellbore damage
- Low Perm (< 0.1 md)
- Small Scale (r_i)

$$\Delta P_{dd} = (1 + S) C_{pf}(\lambda) \frac{Q_t}{M_s} (1 - e^{-t/\alpha})$$

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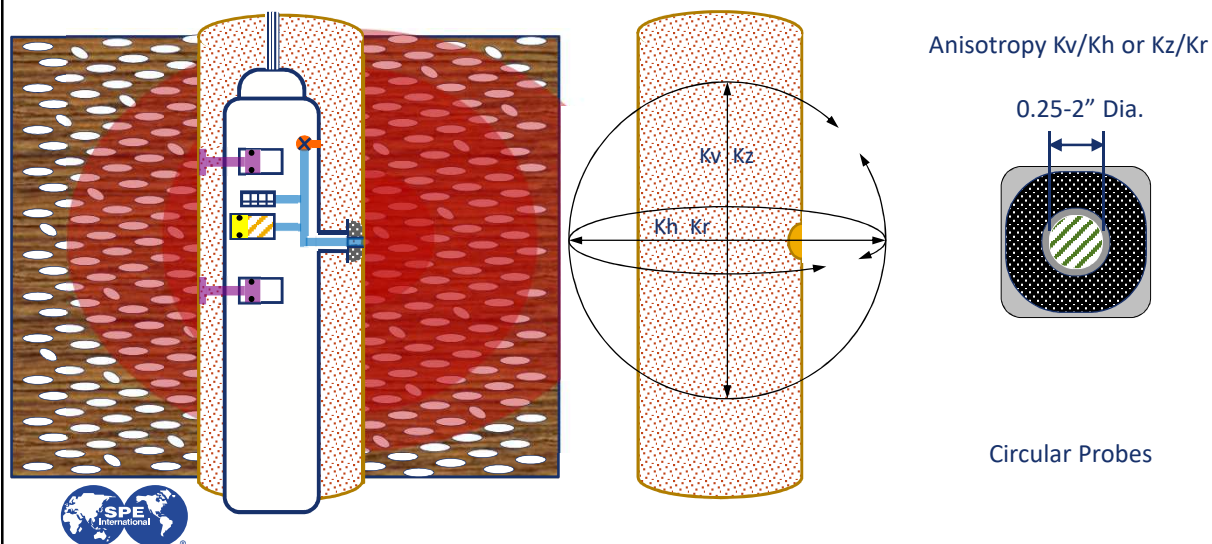
IPTT 3-20+ Hour Tests (MiniDST)

Objective k_h , S , k_v/k_h , h



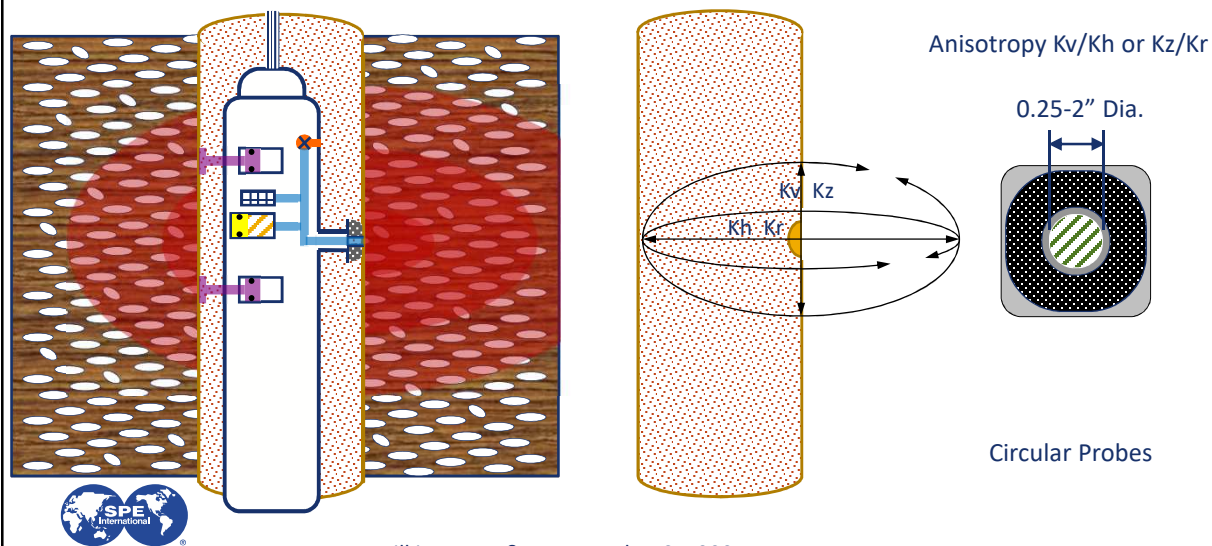
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Typical Formation Tester – Circular Probe



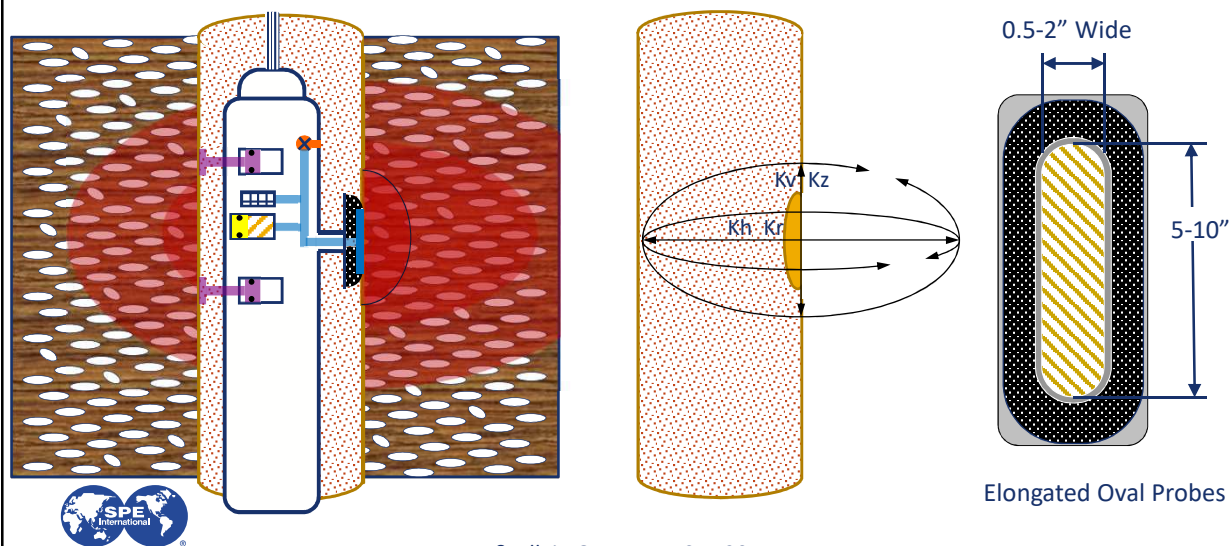
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Typical Formation Tester – Circular Probe



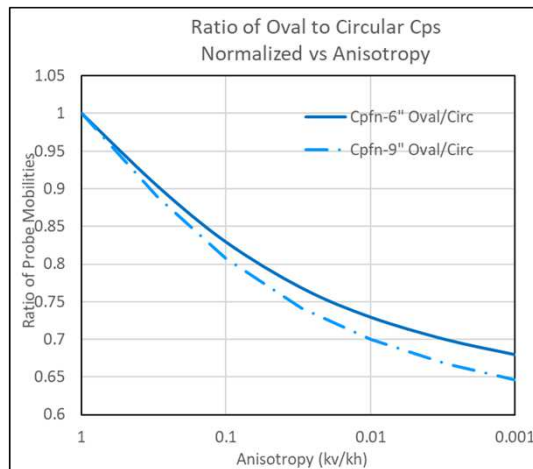
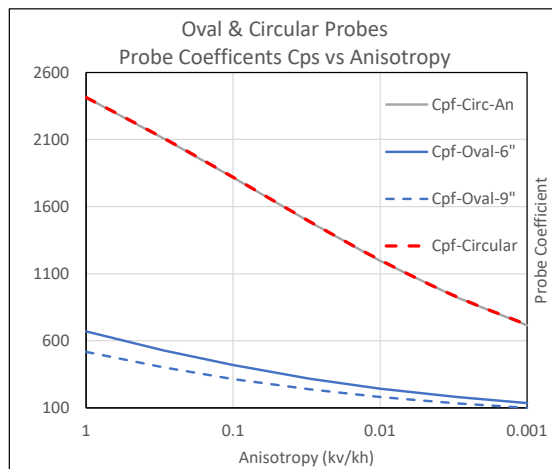
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Typical Formation Tester – Elongated Probe



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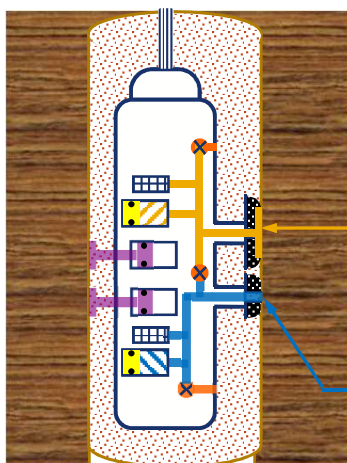
Probe Geometry & Anisotropy Dependency



Larsen, L. & Allain O., SPE 2017 & Wilkinson, D. & Hammond, P. S. 1990

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Pretest Sequence with Oval & Circular Probes



Anisotropy normally assumed to be $k_v/k_h=1$ $\lambda = \left(\frac{M_s}{M_h}\right)^3$

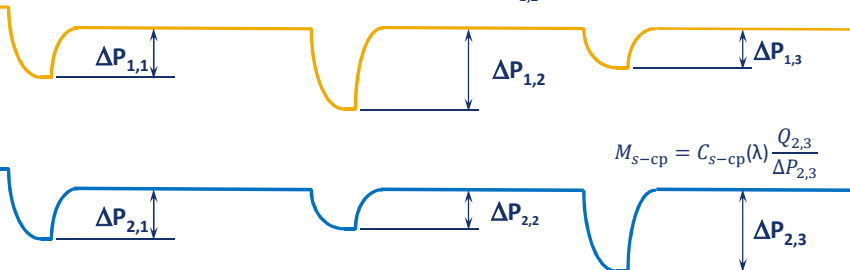
1st Test
Dual Probe Drawdown
 $\Delta P_{1,1} = \Delta P_{2,1} - \text{Source}$

2nd Test
Single Probe Drawdown VIT
 $\Delta P_{1,2} - \text{Source Top Probe}$

3rd Test
Single Probe Drawdown VIT
 $\Delta P_{2,3} - \text{Source Bottom Probe}$

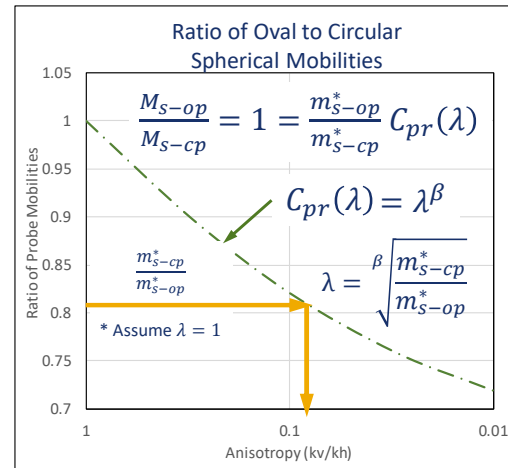
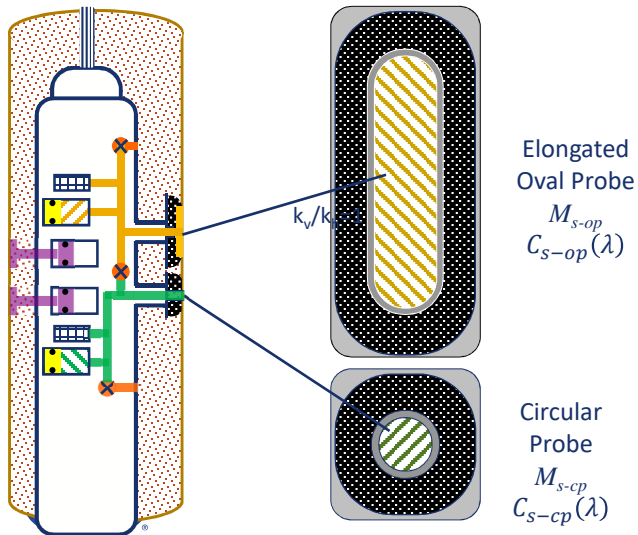
$$M_{s-op} = C_{s-op}(\lambda) \frac{Q_{1,2}}{\Delta P_{1,2}}$$

$$M_{s-cp} = C_{s-cp}(\lambda) \frac{Q_{2,3}}{\Delta P_{2,3}}$$



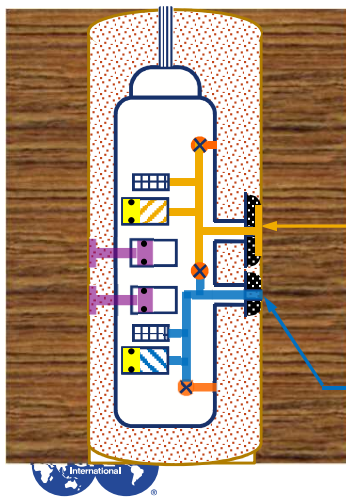
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Formation Tester With Two Probe Shapes

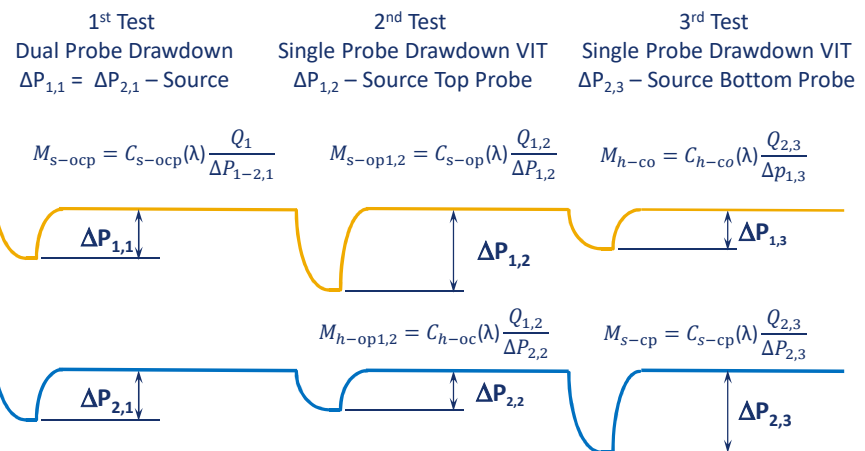


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Pretest Sequence with Oval & Circular Probes

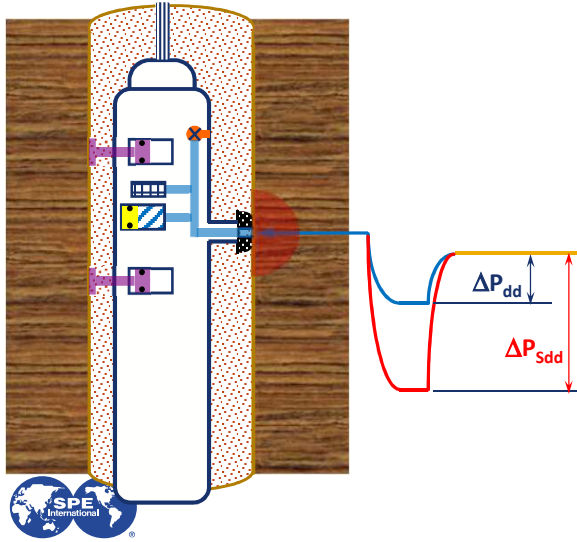


Anisotropy normally assumed to be $k_v/k_h=1$ $\lambda = \left(\frac{M_s}{M_h}\right)^3$



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Considering Near Wellbore Skin



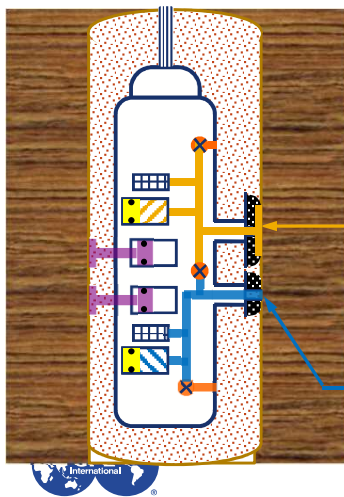
Without Skin

$$\Delta P_{dd} = C_{pf}(\lambda) \frac{Q_t}{M_s} = \frac{1}{4\pi r_p} \frac{Q_t}{M_s}$$

With Skin – Near Wellbore Damage

$$\Delta P_{sdd} = (1 + S_p) C_{pf}(\lambda) \frac{Q_t}{M_s}$$

Pretest Sequence with Oval & Circular Probes



Anisotropy must be assumed due to $C_{pf}(\lambda)$ $\lambda = \left(\frac{M_s}{M_h}\right)^3$

1st Test
Dual Probe Drawdown
 $\Delta P_{1,1} = \Delta P_{2,1} - \text{Source}$

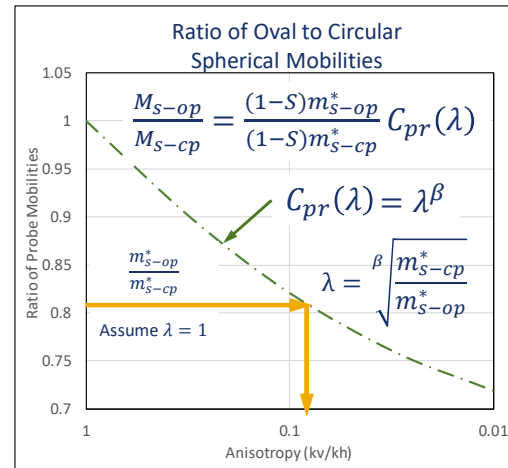
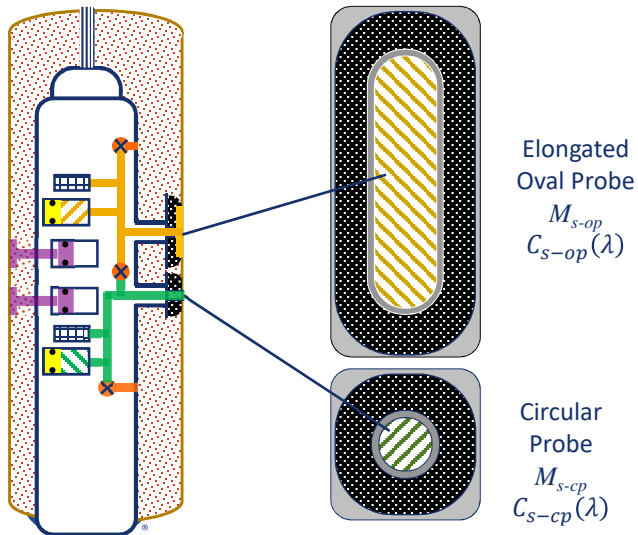
2nd Test
Single Probe Drawdown VIT
 $\Delta P_{1,2} - \text{Source Top Probe}$

3rd Test
Single Probe Drawdown VIT
 $\Delta P_{2,3} - \text{Source Bottom Probe}$

$$m_{s-op1,2} = (1 + S) C_{s-op1}(\lambda) \frac{Q_{1,2}}{\Delta P_{1,2}}$$

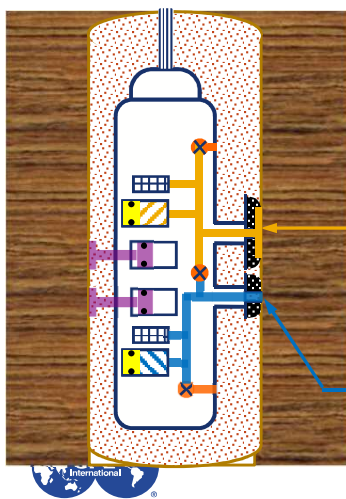
$$m_{s-cp2,3} = (1 + S) C_{s-cp2}(\lambda) \frac{Q_{2,3}}{\Delta P_{2,3}}$$

Formation Tester With Two Probe Shapes



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Pretest Sequence with Oval & Circular Probes



After determining λ and M_h then M_s is determined by $M_s = M_h \sqrt[3]{\lambda}$ and then S

1st Test
 Dual Probe Drawdown
 $\Delta P_{1,1} = \Delta P_{2,1} - \text{Source}$

$$S = \frac{M_{s-op}}{C_{s-op}} \frac{\Delta P_{1-2,1}}{Q_1} - 1$$

$\Delta P_{1,1}$

2nd Test
 Single Probe Drawdown VIT
 $\Delta P_{1,2} - \text{Source Top Probe}$

$$S = \frac{M_{s-op}}{C_{s-op}(\lambda)} \frac{\Delta P_{1,2}}{Q_{1,2}} - 1$$

$\Delta P_{1,2}$

3rd Test
 Single Probe Drawdown VIT
 $\Delta P_{2,3} - \text{Source Bottom Probe}$

$$M_{h-co} = C_{h-co2}(\lambda) \frac{Q_{2,3}}{\Delta P_{1,3}}$$

$\Delta P_{1,3}$

$$M_{h-oc} = C_{h-oc}(\lambda) \frac{Q_{1,2}}{\Delta P_{2,2}}$$

$\Delta P_{2,2}$

$$S = \frac{M_{s-cp}}{C_{s-cp}(\lambda)} \frac{\Delta P_{2,3}}{Q_{2,3}} - 1$$

$\Delta P_{2,3}$

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Solution is Overdetermined



6 – 7 Equations & 3 Unknowns (M_h , S & $\lambda=k_v/k_h$)

$$\frac{M_{s-op}}{M_{s-cp}} = 1 = \frac{m_{s-op}}{m_{s-cp}} C_{pr}(\lambda) = \frac{m_{s-op}}{m_{s-cp}} \lambda^\beta \quad \text{Relationship between two probe geometries}$$

$$\lambda = \sqrt[\beta]{\frac{m_{s-cp}}{m_{s-op}}} \quad \lambda = \sqrt[\beta]{\frac{m_{s-cp}}{m_{s-ocp}}}$$

$$M_{s-ocp} = (1 + S) C_{s-ocp}(\lambda) \frac{Q_{t,1}}{\Delta P_{1-2,1}}$$

$$M_{s-op} = (1 + S) C_{s-op}(\lambda) \frac{Q_{1,2}}{\Delta P_{1,2}}$$

$$M_{h-oc} = C_{h-oc}(\lambda) \frac{Q_{1,2}}{\Delta P_{2,2}}$$

$$M_{s-cp} = (1 + S) C_{s-cp}(\lambda) \frac{Q_{2,3}}{\Delta P_{2,3}}$$

$$M_{h-co} = C_{h-co}(\lambda) \frac{Q_{2,3}}{\Delta P_{1,3}}$$



1 - Solve for anisotropy k_v/k_h

2 - Pressure Test flowing from both circular & oval probes

3 - Pressure Test with oval probe

4 - Circular observation probe interference pressure

5 - Pressure Test with circular probe

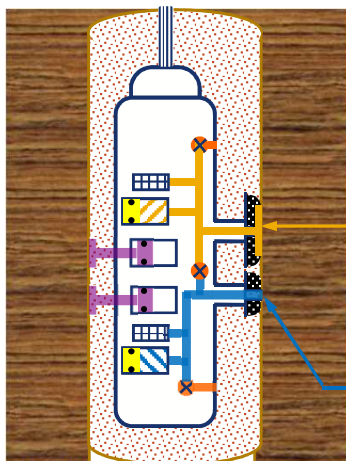
6 - Oval observation probe interference pressure

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Pretest Sequence with Oval & Circular Probes



After determining λ and M_h then M_s is determined by $M_s = M_h^3 \sqrt{\lambda}$ and then S



1st Test
Dual Probe Drawdown
 $\Delta P_{1,1} = \Delta P_{2,1} - \text{Source}$

2nd Test
Single Probe Drawdown VIT
 $\Delta P_{2,2} - \text{Source Bottom Probe}$

$$S = \frac{M_{s-ocp}}{C_{s-ocp}} \frac{\Delta P_{1-2,1}}{Q_1} - 1$$

$$M_{h-co} = C_{h-co2}(\lambda) \frac{Q_{2,2}}{\Delta P_{1,2}}$$

$\Delta P_{1,1}$

$\Delta P_{1,2}$

$\Delta P_{2,1}$

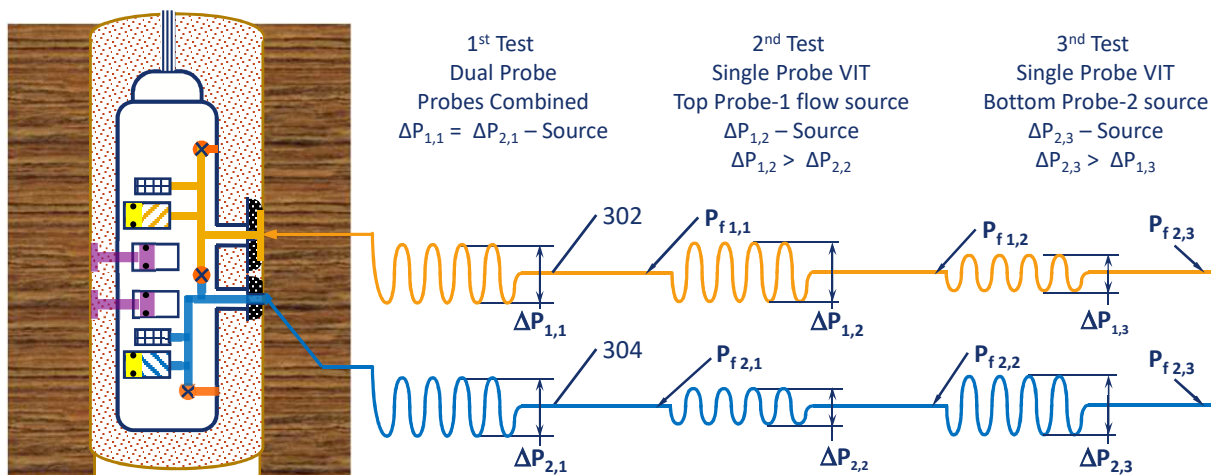
$\Delta P_{2,2}$

$$S = \frac{M_{s-cp}}{C_{s-cp}(\lambda)} \frac{\Delta P_{2,2}}{Q_{2,2}} - 1$$



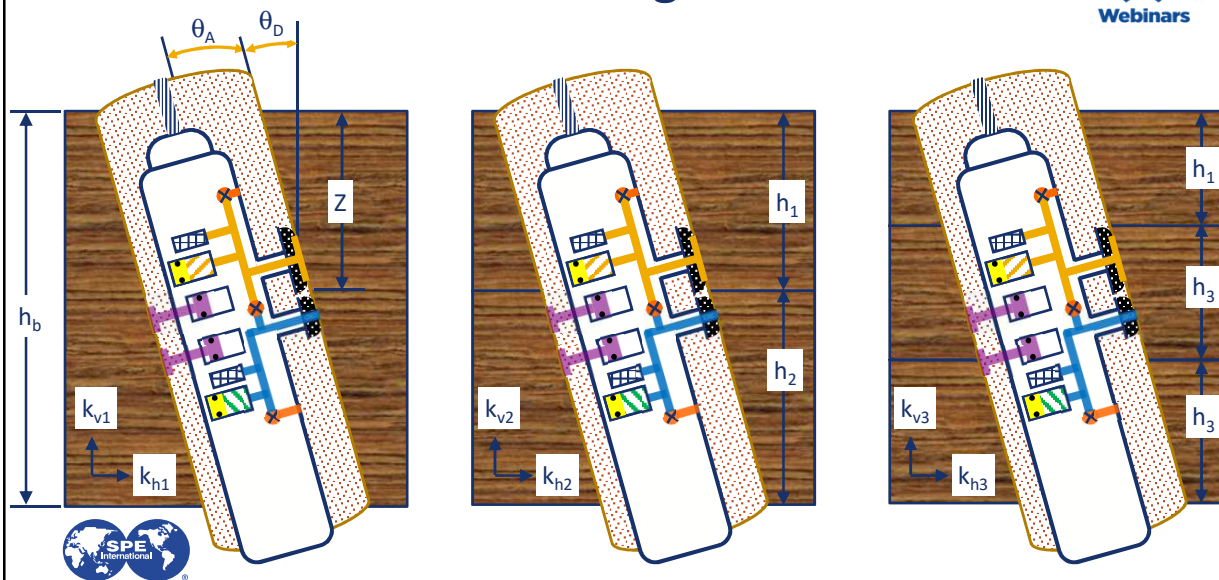
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Pretest with Oscillating Pressure Waves Alternative Testing Method- Low Perm



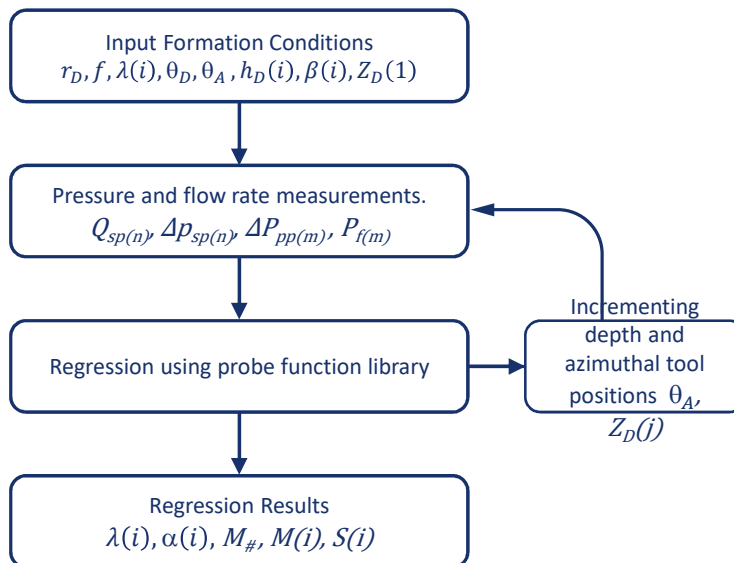
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Formation Heterogeneities



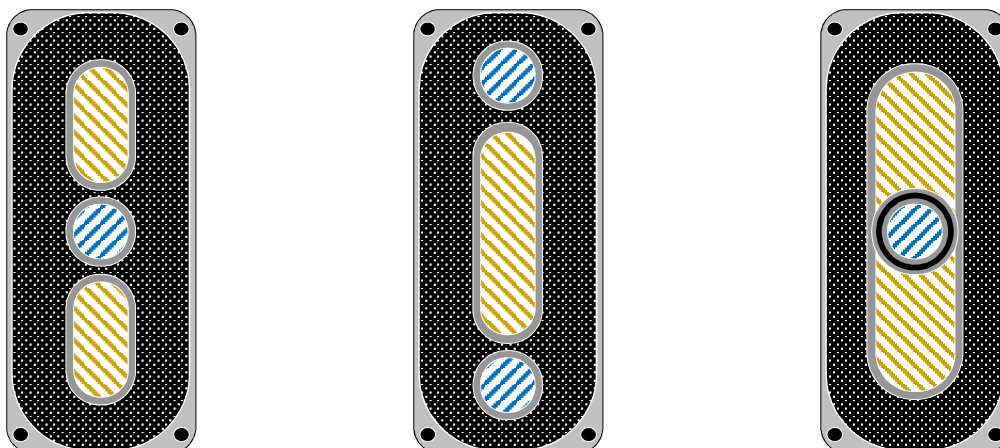
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Multi – Dimensional Solution



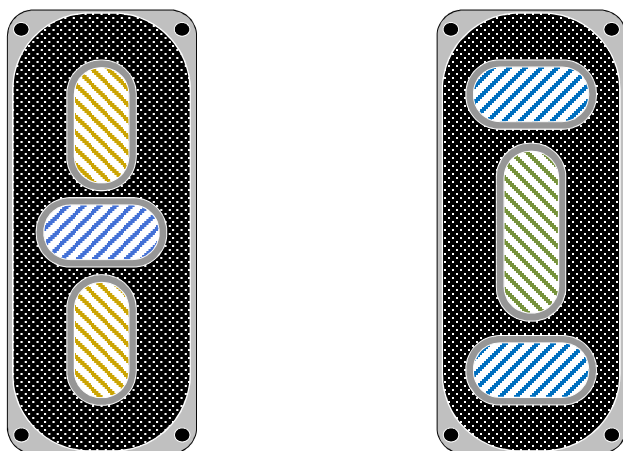
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Enhanced Probe Designs Circular & Oval Shapes



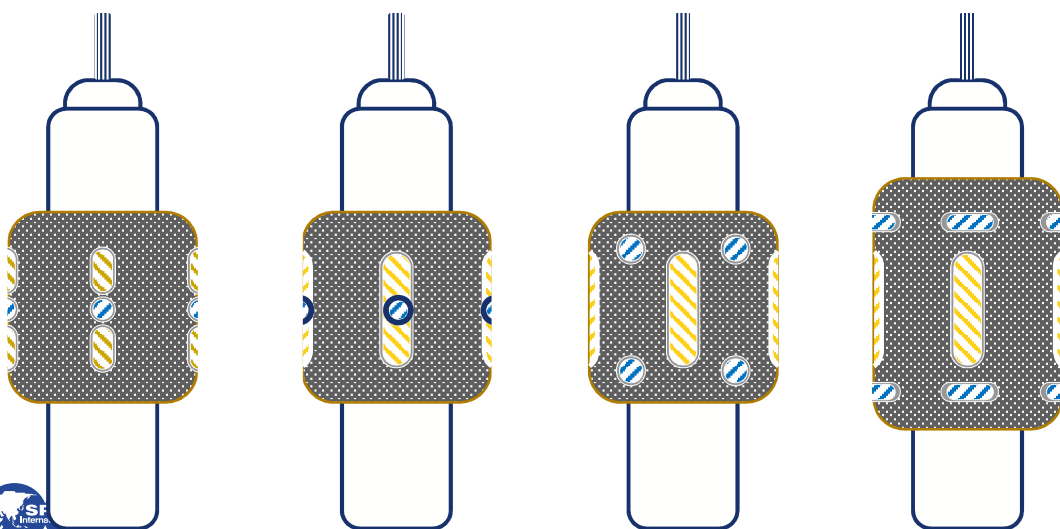
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Probe Designs with Orthogonal Oval Shapes



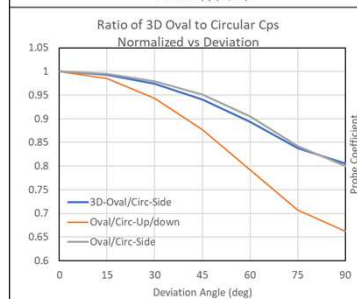
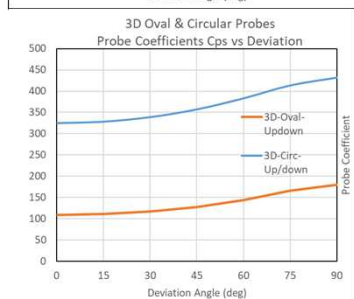
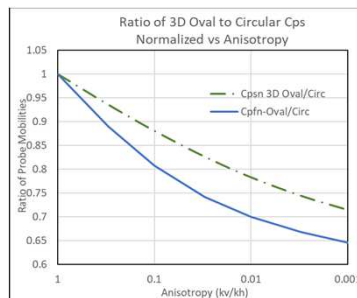
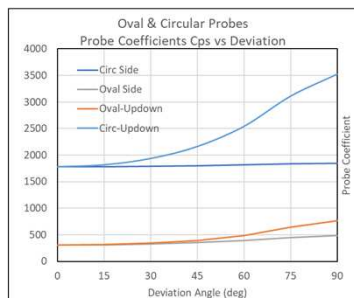
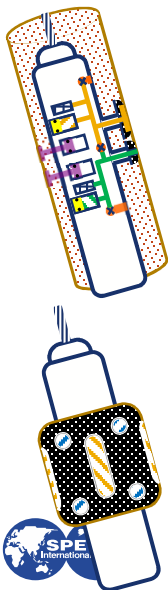
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3D Expandable Probe Designs



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3D Probes vs Single Probes



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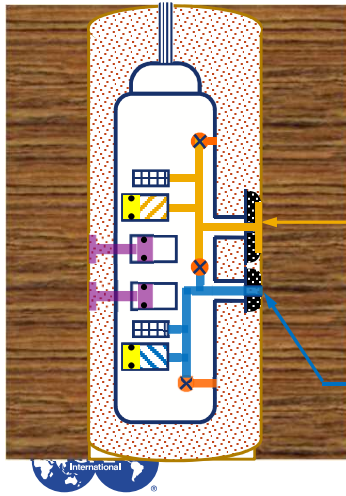
Concluding Remarks

- Using probes of different shapes can enhance pretesting capabilities
 - Skin and Anisotropy can be determined.
 - Greater accuracy for true mobility/perm & anisotropy results
 - Can include the effects of dip angle, azimuthal orientation & heterogeneities
 - 3D Probes can provide a more upscaled measurement
 - New probe designs could improve the sensitivity to anisotropy
- Pretesting methods are unchanged, but generating 10x more data
 - IPTT: Typically, 3-20hrs & not always successful
 - Pretest: Typically, 10-15mins & 10x more tests & data



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Simulation with Oval & Circular Probes



Simulation	Cs-cp	kvkh	Mh	Ms	S
Inputs		0.1	10	4.64	3
	0.84	0.30	9.51	6.37	3.82
		0.10	9.51	4.42	3.10

$$S = \frac{M_{s-ocp}}{C_{s-ocp}} \frac{\Delta P_{1-2,1}}{Q_1} - 1$$

$$S = \frac{M_{s-op}}{C_{s-op}(\lambda)} \frac{\Delta P_{1,2}}{Q_{1,2}} - 1$$

$$M_{h-co} = C_{h-co2}(\lambda) \frac{Q_{2,3}}{\Delta p_{1,3}}$$

 $\Delta P_{1,1}$
 $\Delta P_{1,2}$
 $\Delta P_{1,3}$
 $\Delta P_{2,1}$
 $\Delta P_{2,2}$
 $\Delta P_{2,3}$

$$M_{h-oc} = C_{h-oc}(\lambda) \frac{Q_{1,2}}{\Delta P_{2,2}}$$

$$S = \frac{M_{s-cp}}{C_{s-cp}(\lambda)} \frac{\Delta P_{2,3}}{Q_{2,3}} - 1$$

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