



Live Characterization of Asphaltene Precipitation: Bridging Flow Assurance and Formation Evaluation

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“An **experiment** is a question which science poses to Nature and a **measurement** is the recording of Nature’s answer.”

~ Max Planck

Context



- Flow assurance issues are a costly challenge to mitigate
- Uncertainty exists in characterizing Asphaltene Onset Pressure (AOP)
- A need for a solution to augment lab analysis



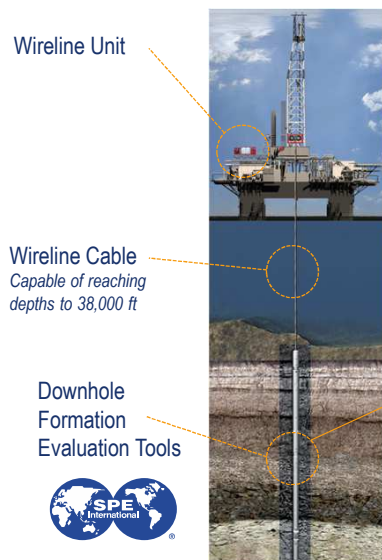
Asphaltene Behavior



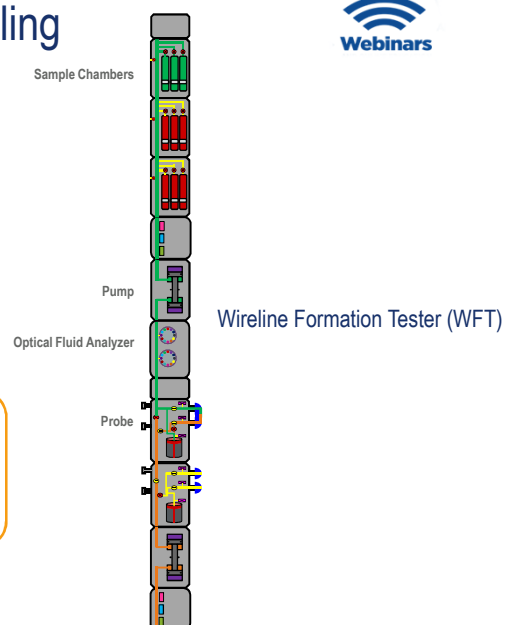
APE: Asphaltene Precipitation Envelope
 UAOP: Upper Asphaltene Onset Pressure
 ARFO: Asphaltene-Resin Flocculation Onset
 BP: Bubble Point
 LAOP: Lower Asphaltene Onset Pressure



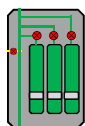
Formation Evaluation: Downhole Sampling



Formation Evaluation data acquired during the Drilling Phase includes
Formation Pressures & Samples

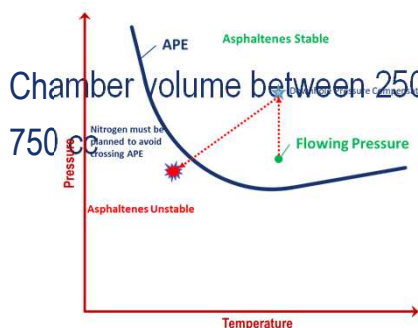


Sample Chamber Module



- Holds PVT Sample Chambers
- Nitrogen compensation *can* preserve samples above APE

- Chamber volume between 250cc to 750cc



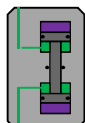
Sample Chambers



Wireline Formation Tester (WFT)



Pump Module



- Cleans sample from mud filtrate to uncontaminated reservoir sample
- Configured according to hydrostatic overbalance



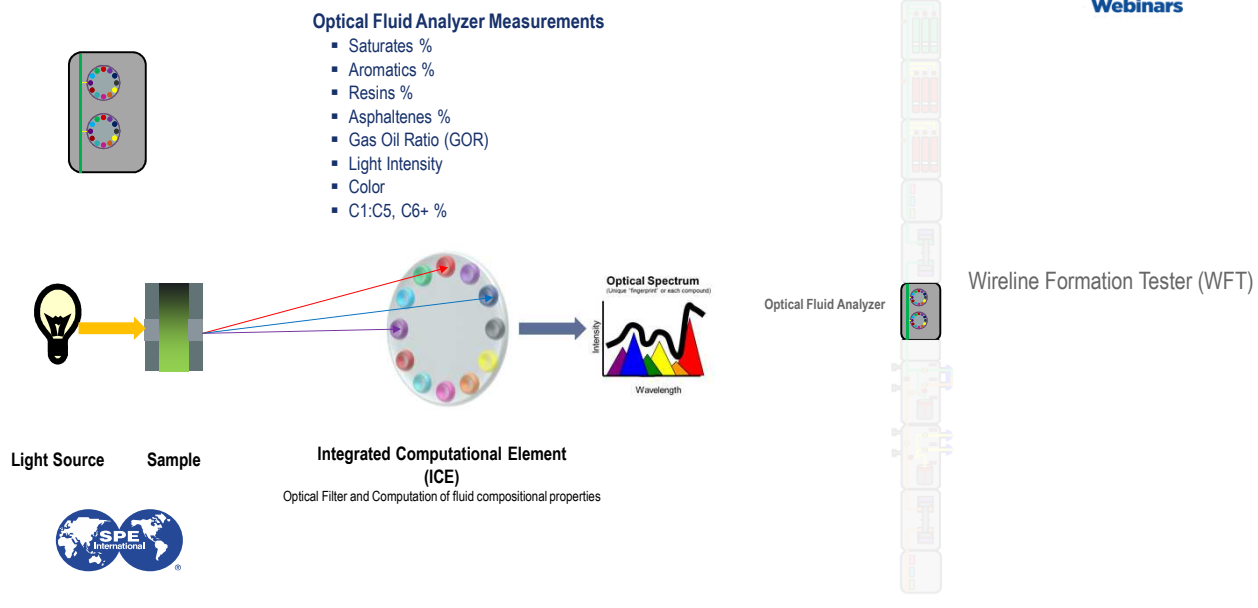
Pump



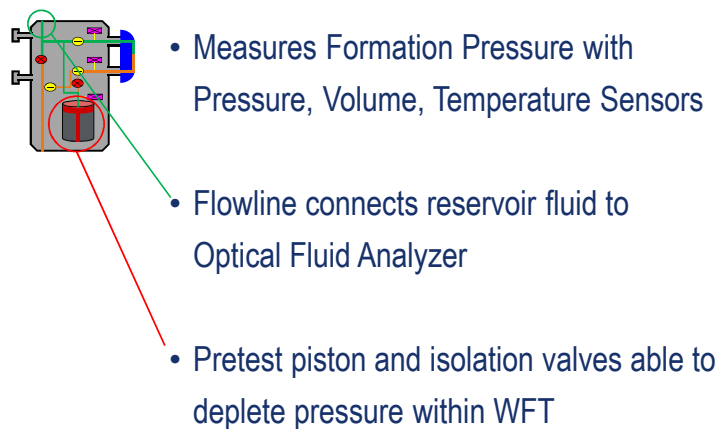
Wireline Formation Tester (WFT)

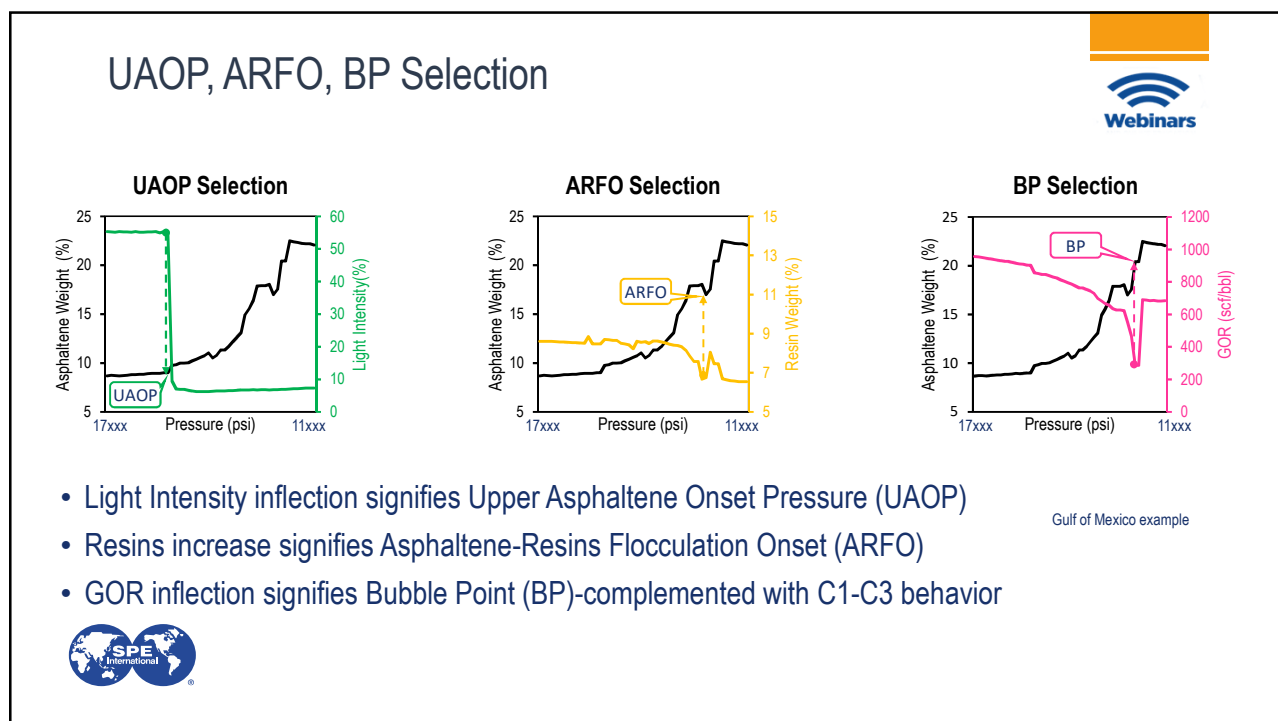
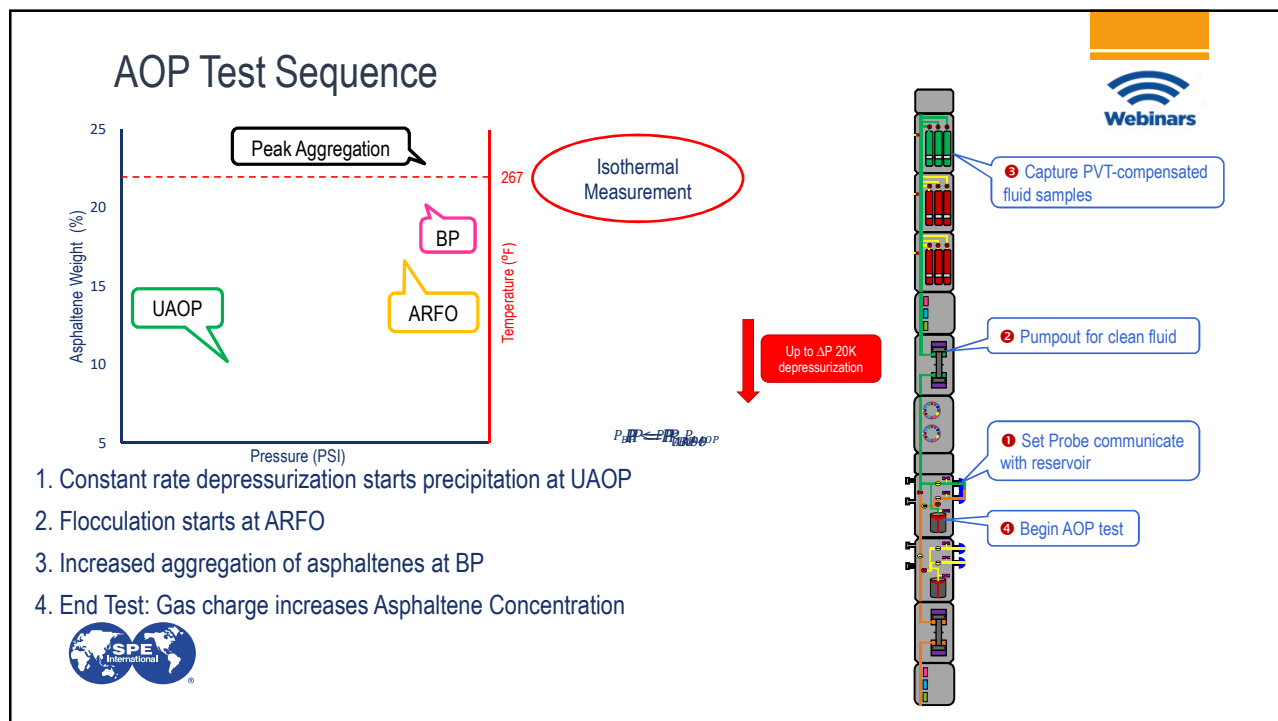


Optical Fluid Analyzer Module



Probe Module





Lab Comparisons



- Downhole AOP values higher than lab indicative of optical sensor sensitivity downhole to detect the onset in-situ
- A value biased higher than the lab is also more risk representative

Downhole AOP (PSI)	Lab (PSI)	Δ(Psi)
13279	12600	679
12631	12300	331
9790	9000	790
10600	10400	200

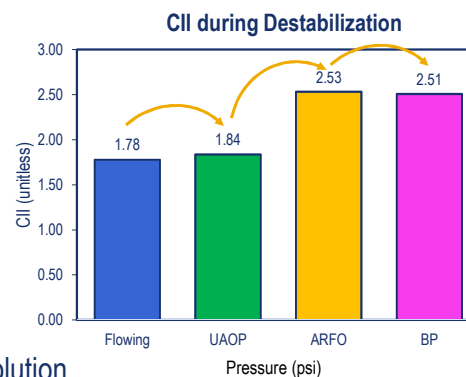


Modeling Method: Colloidal Instability Index



$$CII = \frac{\text{Saturates}\% + \text{Asphaltenes}\%}{\text{Aromatics}\% + \text{Resins}\%}$$

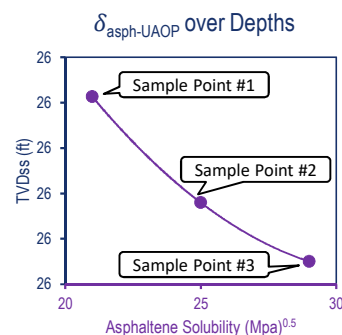
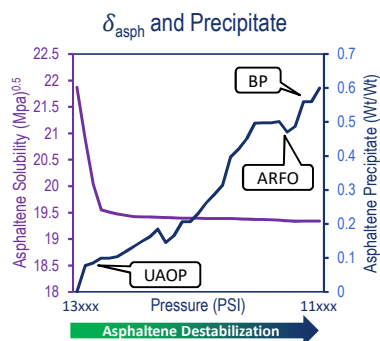
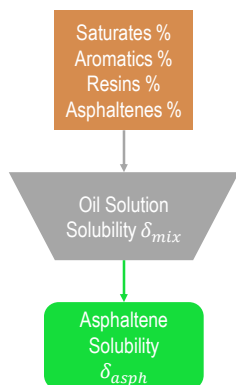
- $CII \leq 0.7$ Asphaltene Fraction stable
 $0.7 \leq CII \leq 0.9$ Asphaltene Fraction uncertain
 $CII \geq 0.9$ Asphaltene Fraction unstable



- CII @ 1.78 indicates higher tendency to precipitate out of solution
- CII values reflect instability as asphaltenes precipitate during destabilization



Modeling Method: Solubility



Gulf of Mexico example

- Resolve reservoir connectivity with asphaltene solubility gradient

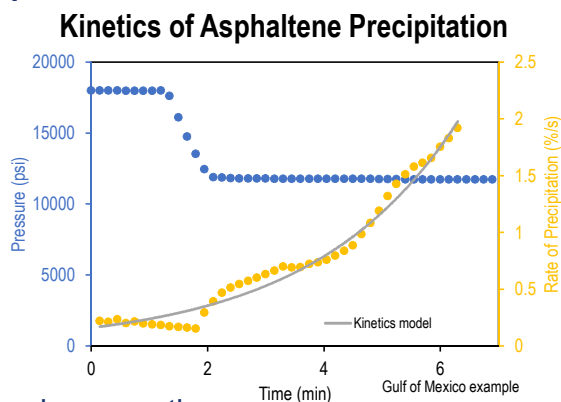


Kinetics of Asphaltene Precipitation



$$\frac{dC}{dt} = k_p (C_0 - C_A^{eq}) e^{k_p \Delta t}$$

$\frac{dC}{dt}$	Rate of asphaltene precipitation
k_p	Precipitation kinetic factor
C_0	Asphaltene concentration in solution pre-precipitate
C_A^{eq}	Asphaltene precipitated concentration
Δt	Incremental time from UAOP

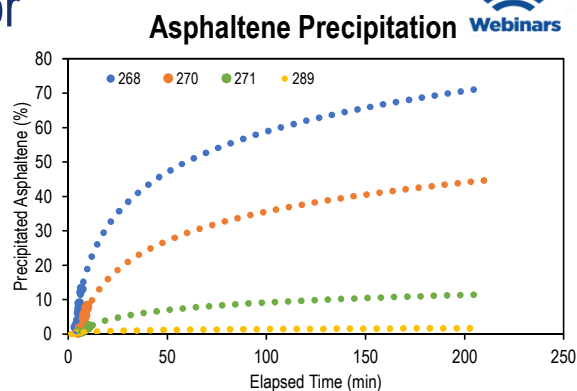


- Describe the rate of asphaltene precipitation and aggregation
- Data honors model



Precipitation Kinetic Factor

Station	Temp. (°F)	$k_p (s^{-1})$
1	268	6.2×10^{-3}
2	270	5.9×10^{-3}
3	271	2.3×10^{-3}
4	289	2.1×10^{-3}



- Lower k_p values support “slower” precipitation rate at higher temperatures
- Corroborates theory of greater stability (equilibrated) at increasing depths
- Validates asphaltene solubility behavior: increase at higher temperatures



Conclusion

- Presented an efficient method to determine AOP downhole during Formation Evaluation
- Demonstrated a way to drastically reduce uncertainty with accurate AOP values
- Illustrated how data can be used to model asphaltene stability, solubility and the kinetics of precipitation



Acknowledgements



- Nikhil Joshi and the SPE Flow Assurance Technical Section
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One Petro: "Enhancing the Understanding of Asphaltene Precipitation: A Novel Approach Under In-Situ Conditions"

